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AFGL- TR-76-0246



INFRARED ABSORPTION BY CH4, H20 AND CO2

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December 1976

Final Report for Period 1 October 1975 - 17 December 1976

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· (14) REPORT DOCUMENTATION PAGE	READ INSTRUCTIONS
1. REPORT DOCUMENT AT 10 2. GOVT. ACCESSION NO	BEFORE COMPLETING FORM 3. RECIPIENT'S CATALOG NUMBER
AFGL TR-76-0246	
4. TITLE (and Subtitio)	5. TYPE OF REPORT & PERIOD COVERED
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INFRARED ABSORPTION BY CHI, Hill and Coll	Final 10/01/75 - 12/17/76
THE RAILED ADDORFT TON DE WAY 172 W 4 2 1	6. PERFORMING ORG. REPORT NUMBER
	U-6275
7. Author(s) David A./Gryvank, J. Dorianne K./Zgonc	
Darrell E./Burch, Dorianne K./Zgonc	F19628-76-C-0067 /
Robert L/ Alt	
9. PERFORMING ORGANIZATION NAME AND ADDRESS	10. PROGRAM ELEMENT, PROJECT, TASK AREA & WORK UNIT NUMBERS
Aeronutronic Ford Corporation	62101F (57)/40
Aeronutronic Division	76700901 (2/)(97)
Ford Road, Newport Beach, CA 92005	
11. CONTROLLING OFFICE NAME AND ADDRESS	12. REPORT DATE
Air Force Geophysics Laboratories (OP)	December 977
Hanscom AFB, MA 01731 Contract Monitor: John E. A. Selby, OPI	84
14. MONITORING AGENCY NAME & ADDRESS(II different from Controlling Office)	15. SECURITY CLASS. (of this report)
Food acrospose and communications	Unclassified
a was special to	154. DECLASSIFICATION/DOWNGRADING
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16. DISTRIBUTION STATEMENT (of this Report)	
Approved for public release; distribution unlimit	ed.
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17. DISTRIBUTION STATEMENT (of the abstract entered in Block 20, If different for	om Report)
18. SUPPLEMENTARY NOTES	
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SECTION 1

INTRODUCTION

BACKGROUND

The primary purpose for the experimental work reported herein has been to provide absorption data to check the Air Force Geophysical Laboratories (AFGL) line-parameter listing and to serve as a basis for possible modification to the listing. The particular absorption bands studied have been selected because of current applications that require that the absorption by these bands in known atmospheric paths be predictable as accurately as possible. Emphasis has been placed on data from which improved values of line intensities, line widths and continuum absorption coefficients can be determined. No new data are reported on line positions because reliable data on the center positions of most of the significant absorption lines are either already incorporated in the AFGL listing or are available elsewhere.

Section 2 provides spectral data on the absorption by CH₄ between 1150 and 1400 cm⁻¹. Absorption in the lower atmosphere by CH₄ is typically much less than that by H₂0 in this same spectral region. However, in the less humid, upper atmosphere, CH₄ produces a large fraction of the absorption that occurs. Because of the complex nate of CH₄ absorption spectra, it is quite difficult to derive a set of CH₄ line parameters from which absorption spectra can be predicted accurately. Recent comparisons of calculated spectra with experimental data indicate that major revisions in the current listing of CH₄ lines are in order. Relative intensities of many of the individual lines can be checked with the detailed data provided in Section 2. The samples investigated cover wide ranges of absorber thickness and pressure with the temperature near 304K.

Some new and improved data are presented in Section 3 on the continuum absorption by pure H₂0 between 600 and 1300 cm⁻¹. Some of these data are believed to be more accurate than similar data reported previously by us. Impurities in the H₂0 samples studied previously may have resulted in values of the continuum absorption coefficient that are too high by as much as 20 percent in some parts of this spectral region. The samples reported in Section 3 varied in temperature from 296K to 430K. The continuum absorption coefficient decreases rapidly with increasing temperatures.

Detailed spectral data are presented in Section 4 on the absorption by H₂0 between 333 and 444 cm⁻¹. Calculating H₂0 absorption in this spectral region from a list of line parameters is complicated by the apparent presence of some continuum absorption in addition to absorption by the lines centered within the region. The data in Section 4 represent samples that cover wide

R. A. McClatchey, W. S. Benedict, S. A. Clough, D. E. Burch, R. F. Calfee, K. Fox, L. S. Rothman, and J. S. Garing, "AFCRL Atmospheric Absorption Eine Parameters Compilation", AFCRL-TR-73-0096, 26 January 1973. (Associated With this report is a magnetic tape listing the line parameters.)

²D. E. Burch, "Investigation of the Absorption of Infrared Radiation by Atmospheric Gases"; Sēmi÷Aṇnual Technical Report, Contract F19628-69-C≡0263, 31 January 1970.

ranges of absorber thickness and pressure, making it possible to determine the relative contribution by the continuum and by nearby lines.

Absorption and emission by the well-known 15 µm bands of CO2 forms the basis for experiments on the remote sensing of the atmospheric temperature profile from satellite-borne instruments. The many overlapping bands in this region make it difficult to calculate accurately the irradiance at the top of the atmosphere, or at a satellite, within any narrow spectral interval in the band system. The extensive data presented in Section 5 are intended to provide a means of checking the intersities, widths, and shapes of the CO2 lines that are involved in the atmospheric calculations. The samples studied cover wide ranges of absorber thickness and pressures from approximately 0.002 atm to l atm. Three sample temperatures, approximately 245 K, 274 K and 310 K, were employed to represent most of the temperature range in the earth's atmosphere. Although temperatures somewhat lower than those employed occur in the atmosphere, the wide temperature range of the samples studied should provide a reliable check on the predicted temperature dependence. Thus, reliable extrapolation to lower temperatures should be possible after the best possible set of line parameters has been derived.

DEFINITIONS, SYMBOLS, AND NOMENCLATURE

The absorber thickness, u, of a gas sample is given by

$$u(\text{molecules/cm}^2) = 2.69 \times 10^{19} \text{ p* (atm) L(cm) } (273/\theta)$$

$$= 7.34 \times 10^{21} \text{ p* L/θ}.$$
(1)

The temperature 0 is in degrees Kelvin, and L is the geometrical path length through the sample. The density-equivalent-pressure p* of the absorbing gas may vary slightly from the partial pressure p at high pressures. The gas does not follow exactly the perfect gas law at the higher pressures for which the Van der Waals' equation of state is required. The deviation from the perfect gas law causes a non-linear relationship between the pressure and the density of the gas. At partial pressures less than 1 atm, p can be substituted for p* without introducing significant error, but p* may differ significantly from p at high pressures. For all of the pressures used in the present investigation, the following simple expression is sufficiently accurate:

$$p* = p(1+c p)$$
 (2)

The pressures are in atm, and c depends on the gas species and temperature. Near room temperature, $c \approx 0.005$ for CO₂, and 0.002 for CH₄. When a sample consists of two or more gas species, the total pressure is represented by P.

The true transmittance that would be observed with infinite resolving power is given by

$$T^{T} = \exp(-u\ell), \quad \text{or} \quad (-1/u) \ln T^{T} = \ell,$$
 (3)

where ℓ is the absorption coefficient. Because of the finite slitwidth of a spectrometer and variations in ℓ with wavenumber due to line structure, the observed transmittance T may differ from T' at the same wavenumber. The quantity T represents a weighted average of T' over the interval passed by the spectrometer.

The absorption coefficient due to a single collision-broadened absorption line at a point within a few cm $^{-1}$ of the line centers, ν_{o} , is given approximately by the Lorentz shape:

$$k_{L} = \frac{S_{J}}{\pi} \frac{\alpha}{(\nu - \nu_{0})^{2} + \alpha^{2}}.$$
 (4)

The line intensity

$$S_{J} = \int k dv \tag{5}$$

is essentially independent of pressure for the conditions of the present study. It has been shown $^3,~^4,~^5$ that for $|\nu-\nu_0|$ greater than a few cm $^{-1},$ the Lorentz equation may require modification. The equation can be modified by employing a correction factor $\chi,$ which is a function of $|\nu-\nu_0|$, so that

$$k = k_{L} \chi = \frac{S}{\pi} \frac{\alpha \chi}{(\nu - \nu_{o})^{2} + \alpha^{2}}, \qquad (6)$$

where k_L denotes the value given by the Lorentz coefficient. The value of χ is approximately equal to unity for small $|\nu-\nu_0|$, but may be quite different for large $|\nu-\nu_0|$. For example, $\chi \ll 1$ for the extreme wings of CO₂ lines,

³D. E. Burch, D. A. Gryvnak, R. R. Patty, and C. E. Bartky; J. Opt. Soc. Am. <u>59</u>, 267 (1969). Also Publication No. U=3203, Philoo-Ford Corporation, Aeronutronic Division, Contract NOnr 3560(00), 31 August 1968.

 $^{^{4}}$ B. H. Winters, S. Silverman, and W. S. Benedict: Journal of Quantitative Spectroscopy and Radiative Transfer $\underline{4}$, 527 (1964).

 $^{^5}$ D. E. Burch, D. A. Gryvnak, and J. D. Pembrook; "The Absorption by $\rm H_2O$ Between 1630 and 2245 cm $^{-1}$ ", Philo-Ford Report U-5090, Contract No. F19628-73-C-0011, January 1973.

but χ may be greater than 1 for H₂O lines. (Ref. 5). Most of the samples in the present study were at sufficiently high pressures for collision broadening to be dominant. Under this condition, the line half-width α is proportional to the collision frequency and thus to the gas pressure. At pressures less than approximately 0.01 atm, the more complex Voigt profile is appropriate.

In many reports and papers, including ones published previously by us, S_J is called line strength. In order to conform with the majority of the workers in the field, we now refer to S_J as the intensity, not the strength. The terms S_V refers to the intensity of a vibration-rotation band that contains many lines. The combined intensity of a system of bands is denoted by S_{SyS} . If essentially all of the absorption in a given spectral region results from a system of overlapping bands, we see from Eq. (3) that

$$S_{SVS} = \int \mathcal{K} dv = (-1/u) \int \mathcal{I} n T' dv.$$
 (7)

Because of differences in the efficiencies of collisions with molecules of different gas species, the half-width of a collision-broadened line depends on the partial pressure of each of the gas species present in a sample. The equivalent pressure Pe given by the following equation is a convenient parameter when dealing with absorption by a mixture that contains non-absorbing No in addition to the absorbing gas species:

$$P_e = Bp + p_{N_2} = (B-1) p + P,$$
 (8)

where P is the total pressure, P_{N_2} is the partial pressure of N_2 , and \hat{p} is the partial pressure of the absorbing gas species. The experimentally determined constant B is the ratio of the self-broadening ability to the broadening ability of N_2 . The equivalent pressure is therefore directly proportional to α , regardless of the relative concentrations of the absorbing gas and the N_2 . We note that P_e approximates P for dilute mixtures of the absorbing gas species in N_2 (p < P $_{N_2}$). The CO_2 samples discussed in Section 5 consisted of CO_2 plus dry air; the dry air consisted of 79% N_2 and 21% O_2 to closely approximate the atmosphere. The same symbol, P_e , represents the equivalent pressure of these samples with P_{air} replacing P_{N_2} in Eq. (8).

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Because of the proportional relationship between α and pressure, k is also proportional to pressure in the extreme wings of a line where $|v-v_0|>>\alpha$. It follows from Eq. (6) that the wing-absorption coefficient C due to the extreme wings of several lines is equal to the sum of all k's due to the individual lines and is proportional to pressure. Because wing absorption changes slowly with wavenumber, it is frequently called continuum absorption. Continuum absorption may also arise from dimers, such as $H_20:H_20$, or from pressure-induced bands. These two types of continuum have the same pressure dependence as absorption by line wings; therefore, in some cases we cannot distinguish which is the source of the absorption being measured. The absorption coefficient due to local lines whose centers occur within a few cm⁻¹ of the point of observation is denoted by $\mathcal{K}(local)$. This quantity may vary rapidly with wavenumber and depends on pressure because of collision-broadening of the absorption lines. At a given wavenumber, there may be absorption by local lines as well as by continuum. Therefore, for a pure H_20 sample, the total absorption coefficient \mathcal{K} in Eq. (3) is given by

$$\mathcal{R} = \mathcal{R}(local) + C_s^o p. \tag{9}$$

The normalized continuum coefficient C_s^o is the value of C_s at a given temperature when p=1 atm. The subscript s denotes self-broadening of the lines. Since α^o is proportional to p, and u is proportional to pL, it follows that $(-L_T)$ for continuum due to the wings of lines is proportional to p^2L .

For a mixture of $\rm H_2O+N_2$, such as several of those used in the present study, Eq. (9) must be modified to account for broadening of the $\rm H_2O$ lines by $\rm N_2$.

$$\bar{R} = R(1ocal) + C_s^o p + C_{N_2}^o p_{N_2}^o.$$
 (10)

Consider the continuum at a wavenumber where the absorption is due to the wings ($|\nu-\nu_0|>>\alpha$) of several lines with the Lorentz shape given by Eq. (4). It follows from the above discussion that C_s^0 / C_{N2}^0 is equal to the ratio α_s^0 / α_{N2}^0 of the normalized half-widths for self-broadening and N_2 broadening. Previous results of measurements at wavenumbers where most of the absorption is due to H_20 lines centered between approximately 1 and 20 cm $^{-1}$ away from the point of the measurement indicate that this ratio is approximately 5. However, at wavenumbers where much of the absorption is apparently due to more distant lines, the ratio C_s^0 / C_{N2}^0 may be much greater than 5. These results indicate that the extreme wings of lines are non-Lorentzian and that the correction factor χ (Eq. (5)) is greater at large $|\nu-\nu_0|$ for self-broadened lines than for N_2 -broadened H_20 lines. Variations in the values of C_s^0 / C_{N2}^0 are discussed in Sections 3 and 4 for H_20 .

SECTION 2

ABSORPTION BY CH₄ BETWEEN 1100 cm⁻¹ AND 1400 cm⁻¹

SAMPLING

The mixtures of $\mathrm{CH_4} + \mathrm{N_2}$ were mixed in a 50-liter, glass-lined mixing tank. The $\mathrm{CH_4}$ was first added to the evacuated tank, and the pressure was measured after the gas in the tank had stabilized. The $\mathrm{N_2}$ was then added, and the resulting mixture was stirred by an internal mixer. The internal blade of the mixer was driven through a rotary seal by a hand-held drill motor. The gases were mixed for approximately 30 seconds, and the mixture was allowed to stabilize before the final pressure was measured. Total pressures of the mixtures were typically 10 atm. The concentration of the mixture was calculated by dividing the pressure of the $\mathrm{CH_4}$ by the total pressure of the mixture with a small correction made for the non-linearity in the relationship between the molecular density and the pressure (see Eq. (2)). Two or three separate batches were mixed for each concentration, and the absorption by a few samples from each batch was measured. The results were compared as a check for the consistency of the mixing procedure.

All of the CH₄ samples for which data are reported were contained in one of two sample cells. The cell lengths are 10.2 cm and 0.574 cm. Each cell had two gas lines attached to it. The gas inlet line was attached to the gas-handling manifold; the other line went to the vacuum pump. The valves and manifold system were arranged so that it was convenient to fill the cell and flush it at nearly constant pressure with a pre-mixed sample of gas. The cell could also be evacuated quickly. The sample cells used for the majority of the data were contained in a vacuum tank that was connected directly to the vacuum tank containing the grating monochromator. The optical path external to the sample cell was evacuated to eliminate interference due to absorption by H₂0 in the atmosphere. A few of the data were obtained a few years ago with the sample cell in an enclosure that was flushed with dry nitrogen.

A typical sampling procedure consisted of filling the evacuated sample cell from a previously mixed batch to a pressure slightly above the desired final pressure. The gas mixture was then allowed to flush slowly through the cell at a nearly constant pressure for several seconds in order to flush out any small amount of air that might have leaked into the gas-handling system. After the cell was flushed adequately, a portion of the mixture was pumped from the sample cell, leaving the desired final pressure for study. Several checks were made for possible errors introduced by leaks or by adsorption of some of the sample gas on the walls of the sample cell or gas lines. The total pressures and absorber thicknesses listed below for the samples are believed to be accurate to less than $\pm 1\%$ and $\pm 2\%$, respectively.

The temperature of the sample cell was measured by a thermometer mounted in good thermal contact with it. The thermometer was read visually through a plexiglass cover on the vacuum tank. Sample cell temperatures varied between

approximately 303 K and 310 K. The cells were not intentionally heated above room temperature; heat from the radiation source and the motor in the vacuum tank increased the internal temperature.

SPECTRAL DATA

All of the CH_{Λ} data except for those in Table 2 are based on spectral curves obtained with the grating spectrometer described previously. 6 The grating used for the CH_{L} data contains 75 grooves/mm and is blazed for maximum efficiency at 12 μm. Overlapping orders of shorter wavelength energy were eliminated by an NaCl prism in the beam just ahead of the grating monochromator. The CH, data in Table 2 were obtained earlier to determine the intensity of the band by employing a commercial grating monochromator (Perkin-Elmer Model E-1) with the optical path flushed with dry nitrogen. The radiant energy from a Nernst glower in either instrument was chopped at 450 Hz to permit amplification and synchronous demodulation of the signal from the detector, which contains a Ge: Cu element cooled by liquid helium. The dc output of the synchronous demodulator was proportional to the amount of chopped energy incident on the detector and was displayed on a strip-chart recorder. A "background" curve was scanned with the sample cell evacuated, either immediately before or after the sample spectrum was scanned. The spectral curve of transmittance for a sample was obtained by comparing the original curve to the corresponding background

Wavenumber calibration was provided from eleven CH₄ lines and seven H₂0 lines of known wavenumber. The CH₄ lines chosen are either unblended, or only slightly blended, so that the positions could be determined with the required accuracy. The H₂0 lines were observed by allowing a small amount of air to enter the vacuum tank that contained the sample cell. It was assumed that each spectrum is linear in wavenumber between each two adjacent calibration lines. Throughout most of the spectral region covered in Figs. 1 and 2, the estimated uncertainty in the wavenumber calibration is less than 0.3 cm⁻¹. The spectral slitwidth for the data in these two figures varies from approximately 0.75 cm⁻¹ at 1170 cm⁻¹ to 1.05 cm⁻¹ at 1400 cm⁻¹. This slitwidth is based on a "triangular" slit function and is equal to the width of the triangle at half-maximum transmission.

Figures 1 and 2 show computer-plotted curves of transmittance for eleven representative samples of $CH_4 + N_2$. The important parameters for each sample are given in the figures. Samples 3 and 4 produce the most absorption, and the corresponding curves cover the widest spectral region. The sample pressures have been varied over a wide range up to 1 atm to provide information on the effect of collision broadening.

At the time the data were obtained, the detector noise was greater than normal. As a result, the rms noise on the recorder tracings corresponded to

⁶D. E. Burch, D. A. Gryvnak, and R. R. Patty. J. Opt. Soc. Am. <u>57</u>, 885 (1967).

⁷NBS Monograph No. 16 (1959).

between 1% and 2% of the signal observed with the sample cell evacuated. The one-second electronic time constant used to reduce the noise necessitated scanning the spectra slowly to avoid errors in regions of rapidly changing recorder deflection. In addition to uncertainties introduced by the noise, the relatively long time required to scan a spectrum increased the possibility of errors due to slow drift that resulted from variations in the source emittance or in the optical alignment. By carefully comparing a complete spectrum with short regions scanned at separate times for an identical sample, we were able to detect and account for most of the significant errors due to drift. Complete spectra of the different samples were also compared for consistency. Areas of inconsistency were re-checked with new samples, and the appropriate changes were made to each spectrum before it was digitized. The digitizing process smoothed-out some of the noise that appeared on the original records.

One apparent discrepancy that was not found until the data were reduced occurs in the spectrum of Sample 3 in Fig. 2. The transmittance values indicated in the figure between approximately 1310 cm $^{-1}$ and 1365 cm $^{-1}$ would be more accurate if they were multiplied by 0.98. The values at lower wavenumbers, between 1250 cm $^{-1}$ and 1310 cm $^{-1}$, may also be too high by a slightly smaller amount. This error probably resulted from placing the background curve too low on the sample spectrum. Some of the small structures in the spectra of the extreme wings of the band are uncertain and may be due to impurities in the sample. Except for the errors noted, the values of transmittance indicated by Figs. 1 and 2 are believed to be accurate to \pm 0.02.

Table 1 shows values of the cumulative integrated absorptance for the samples represented in Figs. 1 and 2. Each column corresponds to the sample indicated at the top of the column. The lower and upper limits of integration depend on the amount of absorption by the sample.

In accordance with Eq. (7), the value of (-1/u) In T' dv over the spectral region including an entire band system is equal to the intensity of the band system. As discussed in Section 1, immediately below Eq. (7), the value of the integral | In T' dv is equal to the experimentally measurable quantity In T dv when the spectral structure is sufficiently wide relative to the spectral slitwidth. A widely used method of measuring band intensities involves measuring the transmittance T for a sample at high pressures so that the individual absorption lines are collision broadened to a width comparable to the spectral slitwidth. Table 2 summarizes the results of such a measurement on a $CH_4 + N_2$ sample at a total pressure of 10 atm and the absorber thickness equal to 6.93 x 10¹⁸ molecules/cm². At this high sample pressure, the lines are broadened so that the transmittance T observed with a 0.8 cm⁻¹ spectral slitwidth is approximately equal to the true transmittance T' that would be observed with infinite resolving power. The value of absorber thickness is sufficiently large to produce measurable absorption throughout most of the band while not producing too much absorption in the strongest portions to be measured accurately. If the transmittance is too low, -In T can not be measured accurately. The results in Table 2 are consistent with results not included that were obtained for other high-pressure samples with different absorber thicknesses.

The combined intensity of all of the lines within a spectral interval is approximately equal to the difference between the two values of the cumulative integral listed in Table 2 for the two wavenumbers bounding the integral. Some allowance must be made for the finite slitwidth and for the contributions by wings of lines. For example, all of the contribution by a line may not be included if its center occurs in the spectral interval of interest but its wings extend outside the interval. The opposite effect results from the extreme wings of lines centered just outside of the interval.

The intensity measured for the entire band system is $574 \pm 25 \times 10^{-20}$ molecules 1 cm² cm⁻¹. This value compares favorably with the previously published values listed in Table 3 below.

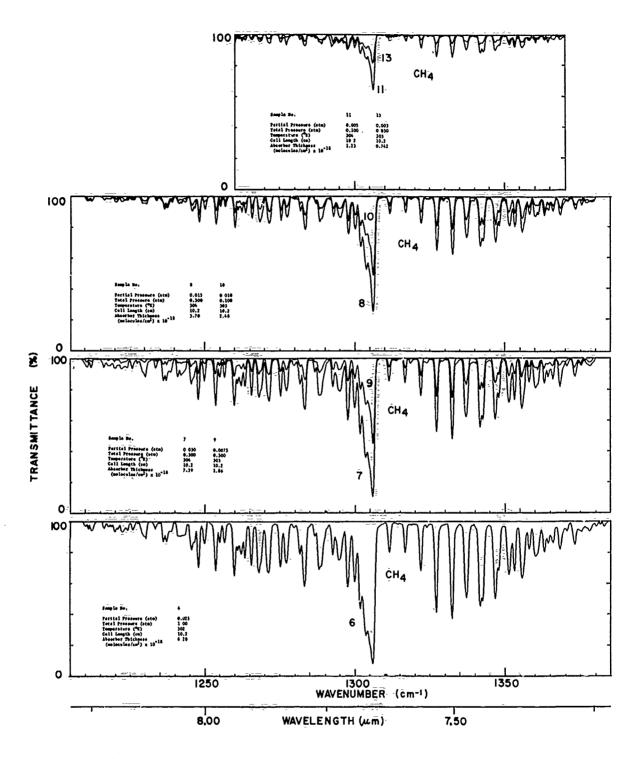
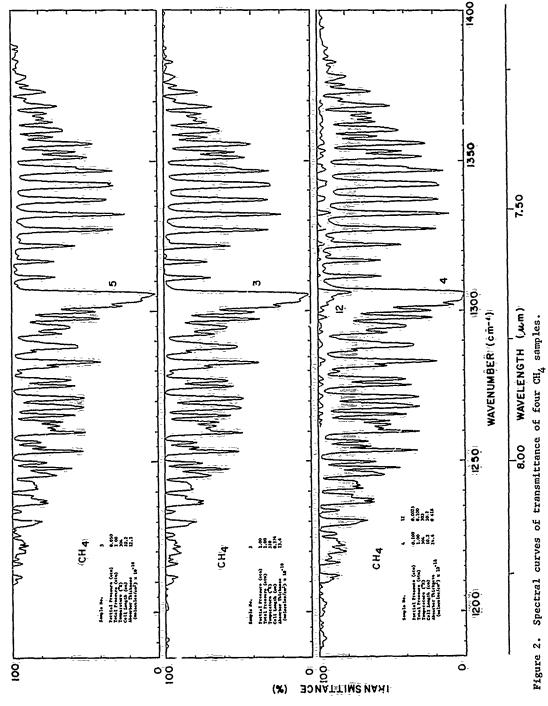


Figure 1. Spectral curves of transmittance of seven CH4 samples.



	Tabl	le I	J	ν (1-Τ) d <i>v</i>			
Sample No.	3	4	5	6	7	8 -	•	10
p-(atm) P (atm) P (atm) Temperature (^O K) Call Length-(cm) u(molecules/cm ²) x 10 ⁻¹⁸	1.00	0.100	0.050	0.025	0.030	0.015	0.0075	0.010
	1.00	1.00	1.00	1.00	0.300	0.300	0.300	0.100
	310_	304	304	302	-304	304	303	302
	0.574	10.2	10.2	10.2	-10.2	10.2	10.1	10.2
	13.6	24.6	12.3	6.20	7.39	3.70	1.86	2.48
(cm ⁻¹) -1185.00 -1186.00 -1187.88 -1188.88 -1189.87	5. 0. 0. 0.000 -0.000	1. 0. 0. 0.604						
1190.00 1191.00 1192.00 1193.00 1194.00	:0.016 07030 0.046 07049 07054	8.842 8.874 9.115 8.141 0.156						
1195.08 1196.08 -1197.00 1198.00	0.055 8.056 0.057 0.058 0.059	0.168 0.183 0.202 (.204 0.228			_			
1200.00 1201.00 1202.00 1203.00 1204.00	0.660 =0.865 0.002 =0.096 0.103	2.249 87273 -0.349 0.354 67385						
-1285.88 1286.88 1287.00 1288.88 1289.88	0.105 -0.115 -0.117 -0.126 0.129	0.398 0.411 0.418 0.425 0.439						
-1210.88 1211.80 1212.00 1213.88 1214.08	0.155 0.206 0.273 0.295 0.296	0.468 0.556 0.663 0.720 0.725	0.016 0.045 0.095 0.119 0.119	8.817 8.846 9.646 3.138 8.135	0:020 0:066 0:104 0:130 0:133	0.004 0.029 0.055 0.071	0.035 0.034 0.034 0.035	0.001 -0.018 0.037 0.049-
1215.80	0.296	0.730	0.119	0.135	6:136	0.072	0.046	0.048
1216.97	0.323	8.762	0.133	0.142	6:168:	0.079	2.046	0.047
1217.80	-0.381	8.868	0.188	0.175	6:193	0.079	0.031	0.045
1218.68	0.416	9.938	0.204	0.179	6:231-	0.116	0.057	-0.045
1219.68	-0.445	1.889	0.227	0.226	-6:271	0.126	0.062	0.043
1220.00	-0.520	1.130	8.274	0.269	0.317	0.151	0.071	0.047
1221.00	0.601-	1.284	8.359	8.319	0.364	0.161	0.000	0.062
1272.00	•0.672.	1.397	8.418	8.354	0.417	0.200	0.093	0.069
1223.00	8.742	1.545	8.588	8.417	0.417	0.231	0.119	0.083
1224.00	-0.814	1.675	8.575	8.463	0.531	0.256	0.139	0.183
1225.00	0.033	1.746	8.684	0.497	6.563	#:268	8.146	8.111-
1226.00	0.000	1.835	8.644	0.530	6.646	9:298	-0.148	8.121
1227.00	0.909	1.896	8.661	0.556	8.638	9:304	8.149	8.133
1228.90	0.911	1.910	8.679	0.561	8.659	9:318	8.149	8.135
1229.00	0.905	2.018	0.748	0.597	8.647	#:335	8.155	8.146
1230.00	1,153-	2.286	0.900	0.645	6.774	-9.386	6.171	0.174
1231.30	1,246	2.528	1.030	0.759	6.859=	9.415	8.164	0.194
1232.00	-1,245	2.546	1.031	0.761	6.873	9.418	8.185	0.199
1233.00	-1,269	2.559	1.035	0.769	6.581-	8.418	8.186	0.288
1234:00	-1,343	2.665	1.086	0.883	6.926	0.439	8.193	0.287
1235.09	:1,353	2.691	1.898	0.815	0-940	0.442	6.200	0.220
1236.00	-1,439	2.792	1.169	0.849	0-973	3.470	0.214	8.249
1237.00	1,681	3.139	1.368	0.957	1-090	0.540	6.243	8.306
1235.00	:1,882	3.458	1.580	1.061	1-209	0.600	6.276	8.352
1239.00	2,918	3.685	1.714	1.123	1-298	0.632	8.282	8.370
1246.60	15847	3.750	1.735	1.143	1,313	9.642	0.284	0.377
1241.80	25158	3.891	1.415	-1.187	1,365	9.667	0.295	0.386
1242.80	25329	4.156	1.941	1.282	1,459	8.710	0.321	0.411
1243.88	27499	4.422	2.136	-1.369	1,556	6.744	0.348	0.431
1244.88	27685	4.613	2.256	-1.441	1,623	r.773	0.369	0.443
1245.00	2.676	4.705	2.318	1.476	1,656	4.743	0.377	0.454
\$245.00	2.963	5.115	2.582	1.632	1,794	8.866	0.418	0.504
1247.00	3.154	5.430	2.780	1.756	1,899	8.927	0.446	0.537
1248.00	3.473	5.818	3.615	1.936	2,059	1.025	0.508	0.645
1249.00	3.588	5.999	3.191	2.845	2,146	1.882	0.535	0.650
1250.08	3:443	6.298	3.364	2.145	21239	1.138	8.556	0.681
1251.00	3:447	6.411	3.448	2.196	21282	1.167	0.569	0.765
1252.08	3:947	5.435	3.459	2.204	21291	1.165	8.569	0.762
1253.00	5:927	6.560	3.525	2.243	21324	1.162	0.571	0.765
1254.05	4:358	7.188	3.919	2.482	21559	1.322	0.646	0.777
1255.00	4:558-	7.411	4.113	2,605	2.666	1.379	0.603	0.809
1256.00	4:663	7.597	4.229	2,676	27729	1.486	0.703	8.825
1257.03	4:838	7.868	4.369	2,752	2.816	-1.448	0.725	8.852
-1259.00	-4:866	7.947	4.430	2,415	2.838	1.457	0.732	8.868
1259.00	4:898	8.018	4.472	2,636	2.858	1.460	0.734	8.862

		Tab	ole I		$\int_{\nu'}^{\nu} (1-$	T) d $ u$	· (c	cont'd	1)		
-gāmpla No.	3	-4	5	6:-	7		•	10	-11-	-12	13
-p (atm)	1.0	-0.100	0.050	0.025	0.030 0.300	0.015 0.300	-0.0075 0.300	0.01d 0.10d	0.005	0.0025 0.100	0.00% 0.030
P-(atm) Temperature (^O K)	1.00- 310	-1.00 304	1.00 304	-1:00 - -302	304	304 10.2	-363 -10.2	302 10.2	304 <u>.</u> 10.2	303 10.2	303 10.2
Cell-length (cm) u(molecules/cm ²) x 10°18	0.574 13.6	10.2 24.6	10.2 12.3	10,2 6,20	10.2 7.39	3.70	1.86	2.48	1.23	0.618	0.742
(cm ⁻¹) 1260.00	5.242	8.483	4.639.	-3.052 3.257	3.653	1.574 1.681	8.801 8.866	0.922 0.974	0. 0.020:	8.817	420.5
-1261.88 -1262.00	5.623 5.931	8.954 9.376	5.149 5.428	3.429	3.371 3.542	1.753	0.913 -0.965	1.812	8.856 8.878	8.831 -8.847	8.822 8.842
-1263.80 -1264.88	6.216. 6.495	9.783 -18.177	5.686 5.949	3.682 3.782	3.641	1.984-	1.020	1.498	8.103	0.867	0.052
-1265.00	6.590	16.322	6.838 6.385	3.832 4.851	3.669 3.851	1.910- 2.813:	1.635 1.103	1.106 1.162	0.106 0.131	0.875 0.898 8.184	6.852 6.871 6.874
1266.88 1267.88	6.95Z 7.024	10.812	6.468	4.109 4.307	3.692 4.020	Z.834- 2.187	1.119 1.172	1.179 1.219	8.142 0.157	0.119	0.083-
-1268.88 -1269.88	7.373: 7.646-	11.362 11.998	6.773 7,213	4.596	4.242	2.255	1.259	1.295	-0-197	0.148	6.105
1270.83	8.020-	12.294 12.679	7.383 7.679	4.713	4.329	2.311 2.384	1.2 86 1.331	1.315	1.223	8.168 8.178	0.112 6.128 8.143
1271.80 1272.00	8.359= 8.822	13.310	8.161	5.201 5.264	4.784	2.541- 2.564	-1.426 -1.442	1.436	8.273: 8.279.	0.198 6.286	0.145
1273.60 1274.88	8.892 8.986	13.463 13.517	8.169 8.190	5.282	4.754	2.564	1.443	1.449	0.279.	6.287	0.145
1275.00	9.067	13.736	8.361	5.378	4.821	2.591 2.702	1.467 1.533	1.469 1.538	8.332 8.332	0.216 0.248	8.152 8.171
1276.00 1277.60	9.418- 9.682	14.618	8.686 8.932	5.603 5.750	5.114	2.765: 2.879	1.568	1.632	0.401 -	-8.255 8.281	0.177 0.191
1278.00 1279.08	10.025 10.067	15.114 15.227	9.247 9.295	5.974. 6.015	5.247 5.314	2.892	1.640	1.641	0.689	A.287	0.198
1288.88	-16.120-	15.349	9.353	6-049-	5.352 5.384	2.983° 2.923	1.645	1.655 1.662	8.411 8.415	8.298 8.294	0.203
1281.08 1282.00	10.162 10.462	15.475 15.858	9.418 9.688	6.856 6.250	5.518	2.991-	1.691 1.756	1.788 2.763	8:437 8:47,4	8.385 0.327	0.209- 0.222
1283.00	18.896- 11.383-	16.392 17. 8 75	-10.054 10.537	6.486 6.834	5.687 5.968	3.896 3.271	1.076	1.468	8.535	0.367	8.268
1285.00	11:451.	17.241	10.606	6.892	5.993-	3.207	1.889	1.893	8.537 8.539	8.375 8.377	8.267 8.276
1286.00 1287.00	11.477	17.315 17.521	10.642	67914 67986	6.069	3.287 3.312	1.985	1.916	8.554 6.581	0.360 8.391	0.264 0.301
1288.00 1289.60	11.925 12.406	17.890 18.536	11.051 -11.499	75141 -75441	6.199 6.433	3,385 3,536-	1.948 2.834	2.036	0.632	4.419	0.334
1298.00	12.683	-18.973	11.765	7÷616	6.565	3.625	2.882 2.896	2.092	1.667 1.67.9	-9.439 8.446	8.361 3.373
1291.80	12.764	19.151 19.257	11.868- 11.926	7.677 7.711	6.685 6.621	3.650 3.662	2.100	2.131	-8.682 -8.715	8.448	8.462
1292. 8 0 1293.09 1294.00-	13.103- 13.334:	19.630	12.196 12.488	:75873 75994 .	6.759 6.865	3.751= 3.822	2.158 2.186	2.193 2.242	8.736	0.486	0.504
1295.00	13.738	28.545	12.784	8,5217	7.059	3.941	2.250 2.318	2.313 2.389	0.775 0.288	0.508 0.527	0.550 1.580
1296.00	14.073- 14.266	21.856 21.342	13.894 13.265	8.410 8.587	7.230 7.327	4.084	2.335	2.412 2.538	1.828 0.887	8.534 0.578	4.629 0.713
-1297.00 1298.00 1299.00	14.821 15.109	22.463	13.786 14.945	8.863 9.032	7.638 7.766	4.274	2.457 2.583	2.597	9.915	0.595	3.763
1300.00	15.582	23.005	14.465	9.296	7.984	4.582	2.588 2.663	2.674 2.763	05964 -13006	6.613 8.639	9.785 9.818
1301.00	16.041 16.726	23.648 24.394	14.885 15.531	9.571 10.016	8.204	4.888-	Z.818	2.917 3.888	1.094	0.686 0.751	ŋ.863 g.92 8
1302.00 1303.00 1304.00	17.539 18.429	25.288 26.253	16.258	18.538 11.241	9.634	5.182 5.619	2.989 3.267	3.327	1.329	0.848	1.000
1305.00	19.369	27.244	18.051	11.979	10.298	6.082 6.722	3.565 4.808	3.606 4.819	1.493 1.769	0.950 1.115	1.882
1306.00 1307.00	20.346 -21.944	28.241 29.198	19.018 19.694	12.844	11.115	7.219 7.253	4.343	4.333	-1*988 -1*994	1.264 1.269	1.335 1.344
1308.00 1309.00	21.159 21.197	29.335 29.425	19.883 19.85 8	13.557 13.582	11.667 11.669	7.263	4.361	4.356	17994	-1.269	1.347
1310.00	21.216	29.478	19.878	13.598	11.669-	7.265	4,363	4.359 4.371	1,994	1,270- 1,272	1.350 1.352
1311.00	21.289	29.578 29.932	19.948 28.191	13.626 13.786	11.691 11.600	7.281 7.366	4.416	4.416	2:031 2:041	1.265	1.363 1.367
1312.00 1313.00	21.567 21.575	30.002	20.230	13.815 13.828	11.814	7.377 7.388	4.425 4.431	4.425 -4.429	2.043	1.288	1.375
1314.00	21.577	30.190	20.293	-13.845	11.637	7.384	4.433	4.431	2:847 2:048	1.285	1.389 1.381
1316.00	21.589 21.815	30.158 30.461	20.325 20.551	13.866	11.845 11.958	7.365 7.458	4.437	4.477	2:866	1.299	1.388
1317.00 1318.00	21.877	30.693	20.631 23.680	14.061 14.083	11.981 12.007	7.478. 7.494	4.497	4.489	2;886 2;085	1.312	1,483
1319.00	21.897	30.747	20.713	14.102	12.016	7.500	4:584	4.499	2.888 2.889	1.319 1.327	1.418
1320.00 1321.00	21.989-	30.812 31.168	20.756 21.053	14.125	12.025 12.165	7.583 7.588	4.567 4.563	4.567	2 119	1.346	1.423
1322.00 1323.00	22.198	31.476	21.251	-14-457	12.260 12.287	7.676 7.690	4.61 8 4.620-	4.616 4.627	2.164 2.166	1.376	1.447
1324.00	22.449	31.582	21.315 21.366	:14.487 14.512	12.384	7.703	4.620	4.642	2,171	1.378	1.449 -1.449
1325.00 1326.00	22.472 22.500	31.666 31.747	21.423	14.535	12.314 12.469	7.713. 7.804	4.62 8 4.679	4.649 4.715	2.177 2.206	1.397	1.475
1327.00 1328.00	22.812 23.362	32.113 32.768	21.734 22.254	15.182	12.801 12.827	8.072 8.100	4.856 4.867	4.458	2:387 2:321	1.458 1.478	1.517
1329.47	23,456	32.931	22.350	15.227			,,,,,,,				-

			Table	ğ: l		, (I-T)dv	(cor	nt'd)		
Sample No.	3	4	5'	- 6	7	8	9	10	-jı	12	13
p (atm) P (atm) Temperature (°E) Cell Length-(cm) u(molecules/cm²) x 10-18	1.00 1.00 310 0.574 13.6	0.100 1.00 304 -10-2 24.6	0:056 1:00 304 10:2 12:3-	0.025- 1.00 302 10,2 6,20	0.030 0.300 304 10.2- 7.39	0.015 9.330 334 10.2 3.70	0,0075 0,300 303 10,2 1786	0.010 0.100 302 10.2 2.48	0.005 0.100 304 -10.2 1:23	0.0025 0.100 303 10.2 0.618	0.603 0.03d 305 10.2 0.742
(cm 1)		_	_				4.869	4.883	2.324	1.474	1.527
1330.00 1331.00 1332.00 1333.00 3334.00	23.496 23.531 23.815 24.686	33.026 <3.114 43.494 34.284 34.521	22.405 22.459 22.753 23.408 23.551	15.24? 15.268 -15.485 -16.008 -16.100	12.841. 12.852 12.982 13.483 13.461	8.121 8.128 8.197 8.515 8.578	4:870 4:922 5:126 5:148	4.893 4.943 5.113 5.143	2.326 2.358 2.465 2.493	1.475 1.487 1.560 1.578	1.527 1.542 1.590 1.602
1335.00 1336.00 1337.00 1338.02 1339.00	24.728 26.784 25.203 25.806 25.941	34.625 34.743 35.323 36.002 36.185	23.601 23.674 24.114 24.655 24.774	16.126 16.157 16.443 16.851 16.919	13.479- 13.496 13.752 14.048- 14.086	8.587 8.601 8.735 8.961 9.010	5:149 5:151 5:248 5:381 5:394	5.145 5.149 5.238 5.363 5.384	2.495 2.502 2.552 2.625 2.638	1.571 1.571 1.600 1.650 1.550	1.603 1.603 1.631 1.671 1.678
1340.60 1341.00- 1342.00 1343.00	25.995 26.109 26.694 27.395 27.666	36.304 36.524 37.249 38.025 38.306	24.828 24.950 25.538 26.190 26.415	-16.944 -17.012 -17.450 -17.943 -18.086	14.113- 14.152 14.504. 14.880= 14.987-	9.033 9.865 9.310 9.587 9.688	5.394 5.407 5.567 5.738 5.781	5.391 5.406 5.539 5.698 5.762	2.641 2.654 2.735 2.833 2.878	1.659 1.668 1.713 1.774 1.795	1.683 1.691 1.738 1.786 1.803
1345.00 1346.00 1347.00 1348.00	27.720 27.638 25.436 26.970 29.213	38.429 38.651 39.409 40.047 40.328	26.484 26.619 27.183 27.679 27.914	:18.116 18.191 18.597 -13.939 19.096	15.004 15.049- 15.372 15.631 15.751	9.791 9.735 9.962 13.161 10.265	5.784 5.800 5.930 6.644 6.090	5.773 5.799 5.929 6.643 6.101	2.580 -2.887 2.964 -3.036 3.078	1.796 1.891 1.844 1.887 1.912	1.895 1.895 1.843 1.877 1.895
1350.80 1351.90 1352.00 1353.00	29.259 29.504 29.993 33.324 30.611	40:434 40:820 41:458 41:878 -42:248	27.968 28.205 28.654 28.946 29.236	-19.130 19.282 -19.577 19.776 -19.971	15.768- 15.889 16.434 16.279= 16.438=	10.257 10.358 10.517 10.629 10.753	6-095 6-137 6-232 6-287 6-354	6.113 6.172 6.256 6.303 6.372	3.084 3:102 3.152 3.156 3.230	1.913 1.929 1.966 1.999 2.038	1.897 1.908 1.940 1.965 2.003
1355.00 1356.00 1357.00 1358.00	30.749 31.286 31.646 31.839 32.805	42:548 43:108 43:6:7 43:880 46:133	29.361 29.846 33.198 30.374 30.558	20.052 20.378 20.651 20.710 20.823	16.480- 16.765 16.936- 17.020 17.101	10.794 17.992 11.131 11.198 11.266	6±369 6±469 6±524 6±552 6±586	6.414 6.538 6.622 6.677 6.716	3.244 3.318 3.361 3.377 3.395	2.049 2.091 2.130 2.158 2.191	2.025 2.067 2.093 2.116 2.137
1360.00 1361.00 1362.00 1363.00	32.270 32.629 32.779 32.967 33.218	44.521 45:035 45:275 45:550 45:678	30.771 31.113 31.271 31.452 31.668	20.964 21.179 21.294 21.413 21.553	17.208 17.367 17.464 17.533 17.651	11.353 11.467 11.524 11.597	61629 61693 61726 61771 61816	6.749 6.803 6.838 6.878 6.942	3.419 3.438 3.449 3.465 3.488	2.219 2.259 2.289 2.321 2.361	2.158 2.177 2.190 2.199 2.212
1365.00 1366.05 1367.00 1368.00	33.425 33.637 33.727 33.883 34.156	46.191 46.511 46.673 46.896 47.324	31.864 32.068 32.176 32.329 32.599	21.673 21.791 21.865 21.947 22.698	17.749 17.849 17.961 17.957 18.186	11.746 11.818 11.854 11.905 11.998	67851 68893 67912 6.937 67977	6.985 7.030 7.753 7.091 7.153	3.515 3.538 3.555 3.567 3.591	2.396 2.419 2.439 2.458 2.495	2.228 2.234 2.234 2.243 2.253
1379.00 1371.00 1372.00 1373.00	34.268 34.338 34.356 34.510 34.673	47.521 47.685 47.749- 47.995 48.271	32.720 32.821 32.866 33.346 33.724	22.159 22.214 22.233 22.319 22.426	18.169 18.203 18.218 18.274 18.367	12.035 12.758 12.061 12.101 12.1 <i>c</i> 2	7:000 7:318 7:021 7:053 7:099	7.170- 7.195 7.209 7.236 7.283	3.598	2.521-	2.255
1375.67 1376.00 1377.00 1376.00	34.727 34.788 34.812 34.877 34.941	48.394 48.538 48.634 48.807 48.952	33.306 33.391 33.445 33.544 33.629	22.483 22.542 22.582 22.634 22.681	18.398 18.435 18.456 18.508 18.543	12.186 12.224 12.257 12.259 12.313	7.119 7.143 7.152 7.170 7.193	7.393 7.320 7.338 7.362 7.394			
1380-00 1381-09 1382-00 1383-00	34.952 34.972 34.992 35.035 35.068	49.027 49.116 49.198 49.310 49.382	33,667 33,694 33,733 33,782 -33,819	22,791 22,722 22,736 22,758 22,771	18.561 18.561 18.561 18.561 18.561	12.325 12.325 16.325 -12.325 •2.325	7:196 7:196 7:196 7:196 7:196	7.411 7.411 7.411 7.411 7.412			
1385.00 1386.00 1387.00 1388.00	35.087 35.099 35.106 35.128 35.133	49:455 49:515 49:576 49:650 49:698	33.846 -33.882 -33.928 -33.967 -33.991	22.772 22.772 22.772 22.772 22.772	18.561.	12.325	7 -19 6	7.41Z			
1390.00 1391.00 1392.00 1393.00	35.140 35.141 35.142 35.145 33.149	49.748 49.774 49.805 49.835 49.868	33.991 33.991 33.991 33.991 33.991	22-772 22-772 22-772 22-772 22-772							
1395.00 1396.00 1397.00 1398.00 1399.00	35.161 35.163 35.167 35.169 35.179	49.912 49.038 49.968 50.007 50.032	33.991 33.991 33.991 33.991 33.991	22.772 22.772 22.772 22.772 22.772							
1400.00	35.188	Šā.056	33.391	22.772							

TABLE 2 $\frac{1}{u} \int_{v}^{v} -\ln t \, dv$ FOR CH_4

(Multiply all integral values by 10^{-20} molecules $^{-1}$ cm 2 cm $^{-1}$)

ν (cm ⁻¹)	$= \frac{1}{u} \int_{v}^{v} - \ln x dv$	v (cm ⁻¹)	$-\frac{1}{u}\int_{v'}^{v}-\ln t dv$
-(cm)-		(cm. ·)	
12 10	-0.72	1285	151.6
1215	3.04	1290	167.9
1220	6.17	1295	181.3
1225	10.54	1300	207.3
1230	14.26	1305	288.1
1235	18.23	1310	350.4
1240	25 . 73	1315	358.9
1245	33.19	1320	366.0
1250	47.26	1325	376.8
1255	57.63	1330	399.1
1260	68.58	1335	426.3
1265	86.30	1340	447.5
1270	104.9	1345	478.3
1275	120.8	1350	502.8
1280	134.6	1355	524.0

 $v^{i} = 120\overline{5} \cdot cm^{-1}$

When the wings of the band are included in the integral, the value becomes 574 ± 25 x 10^{220} molecules 1 cm² cm⁻¹, which is equal to the value of the intensity of the entire band system.

TABLE 3. COMPARISON OF EXPERIMENTAL VALUES OF BAND INTENSITY

	-(-1:/u) _ √T đy
Reference	_(molecules -1 cm cm -1)_
Rollefson and Havens	551×10^{20}
Thorndike 9	558 x 10 ²⁰
Welsh and Sandiford	585×10^{20}
Armstrong and Welsh	588 x 10 ²⁰
Present Investigation	574×10^{20}

^{8.} R. Rollefson and R. Havens, Phys. Rev. 57, 710 (1940).

^{9.} A. M. Thorndike, J. Chem. Phys. 15, 868 (1947).

^{10.} H. L. Welsh and P. J. Sandiford, J. Chem. Phys. 20, 1646 (1952).

^{11.} R. K. Armstrong and H. L. Welsh, Spectrochimica Acta 16, 840 (1960).

SECTION 3

CONTINUUM ABSORPTION BY H20 BETWEEN 600 cm 1 AND 1300 cm

The absorption by H₂0 in the atmospheric window between approximately 800 cm⁻¹ and 1200 cm⁻¹ is different from that in most regions because a significant portion of it is due to continuum absorption. Although many very weak H₂0 lines are centered in this region, the contribution by these lines in a typical lower atmospheric path is much less than that by the continuum. Some of the continuum absorption is undoubtedly due to the extreme wings of strong H₂0 lines centered outside of the 800 - 1200 cm⁻¹ interval. Dimers formed by the association of two H₂0 molecules (H₂0:H₂0) may also contribute to the continuum absorption. For purposes of calculating the attenuation by atmospheric paths it is not important that the absorbing mechanism be understood completely as long as the absorption coefficients at different wavenumbers are determined for temperatures and pressures of interest. As explained in Section 1, the attenuation over a given path length varies as the square of the H₂0 partial pressure whether the absorption is due to dimers of to the extreme wings of self-broadened H₂0 lines.

Within the 600 - 1300 cm⁻¹ region there are several narrow intervals as wide as approximately 1 cm⁻¹ at which the influence of lines closer than a few cm⁻¹ is much less than that by the continuum absorption. Throughout much of the more transparent part of the window between 800 cm⁻¹ and 1200 cm⁻¹, there is probably little contribution by all of the lines centered closer than 30 = 50 cm⁻¹ to many of these narrow intervals between very weak nearby lines. Lines centered in the edges of the window from 600 cm⁻¹ to 800 cm⁻¹ and from 1200 cm⁻¹ to 1300 cm⁻¹ are stronger than those in the center of the window. Co sequently, nearby lines can make a significant contribution to the absorption in the narrow, clean intervals in these edges of the window. Nevertheless, the continuum still plays a very important role in these intervals.

In 1970 we published a report that included data on the H_2O continuum absorption throughout the 700 = 1250 cm⁻¹ region. The continuum absorption was determined by measuring the absorption in several of the narrow, clean intervals discussed in the previous paragraph. The absorption was measured from spectral curves of transmittance scanned with a spectral slitwidth of less than 0.5 cm⁻¹. By making a small allowance for a few nearby lines, the continuum was determined for samples at different pressures and temperatures. Values of the continuum absorption coefficient C_S^O (see Eq. (10)) for self-broadening were determined and published for three temperatures: 296 K, 358 K and 388 K. Attempts to measure the nitrogen broadening coefficient C_{N2}^O as part of the same experiment were unsuccessful because of the very weak dependence of the continuum absorption on the pressure of N_2 . However, the results did indicate that near room temperature the ratio C_{N2}^O is less than 0.005.

Since publishing these original data on the $700 = 1200 \text{ cm}^{-1}$ region, we have investigated the continuum absorption in other spectral regions and have

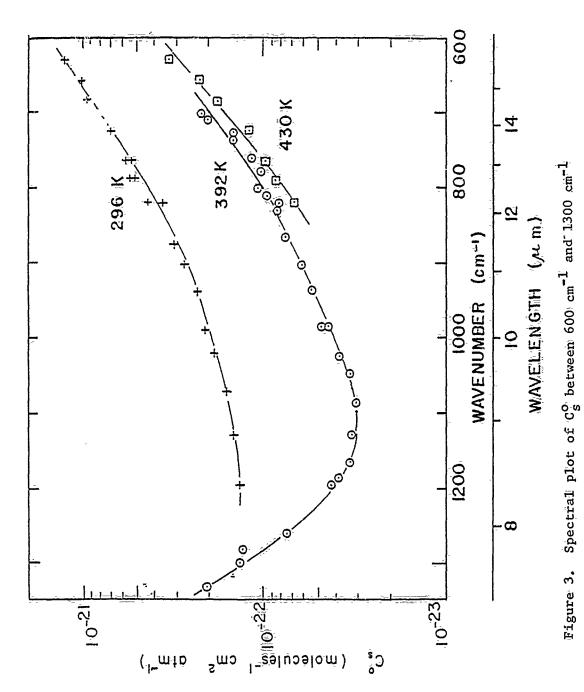
improved some of our experimental techniques. Because of the importance of the 700 - 1250 cm⁻¹ region, we have re-investigated the continuum absorption while employing some of our improved techniques, particularly those related to interference by contaminants in the sample. As a result of the more recent measurements, we have concluded that the previously published values of C_S were probably too high by 5% to 20%. The highest percentage error is between 1000 cm⁻¹ and 1200 cm⁻¹ where absorption by contaminants was the most serious. This amount of discrepancy between two separate measurements is believed to be quite good in view of the difficulty of the experiment.

Figure 3 summarizes the results of the later measurements. The uncertainty in the results is difficult to estimate because of the possibility of some systematic experimental error that is not identified. However, we believe that any of the values represented by the 296 K curve are in error by less than \pm 15%, and those for the two elevated temperatures, 392 K and 430 K, by less than \pm 10%. The large decrease in $C_{\tilde{S}}^{0}$ with increasing temperature is consistent with the previous data.

At 392 K, Co increases rapidly with increasing wavenumber above approximately 1950 cm⁻¹. The intensities of the H₂O lines centered in or near the 1150 cm⁻¹ - 1300 cm⁻¹ region increase rapidly with increasing temperature because the lower energy levels involved in the transitions are excited. The populations of these energy levels therefore increase rapidly with temperature. The increase in Co is a result of the increasing contribution by the lines centered above 1150 cm⁻¹. The contribution by these same lines is apparently small for wavenumbers less than 1100 cm⁻¹. A large portion of the continuum below 1100 cm⁻¹ is probably due to the extreme wings of the very strong lines centered below 600 cm⁻¹. This could account for the increasing Co with decreasing wavenumber below 1100 cm⁻¹ as the point of observation approaches these strong lines.

Singe being published, the 1970 data have been used widely to predict atmospheric absorption and have been compared with results of a variety of experiments. The more recent data illustrated in Figure 3 have also been made available to a few workers interested in developing accurate transmission models. Among these workers are Roberts, Selby and Biberman, 12 who have summarized the results of several field measurements and laboratory measurements designed to provide new and better information on the H₂O continuum absorption. Roberts, et al., have arrived at what they believe is the best model for continuum absorption based on the variety of data they have accumulated. Their model is in essential agreement with Fig. 3 for 296 K.

¹² R. E. Roberts J. E. A. Ṣēlby and L. M. Biberman, Appl. Opt. 15, 2085 (1976).



SECTION 4

ABSORPTION BY H₂0 BETWEEN 333 cm⁻¹ AND 444 cm⁻¹

EXPERIMENTAL

The H₂O absorption data presented in this section were obtained in the same manner as the H₂O data reported previously by us in several reports. The longer of two multiple-pass cells in our laboratory was used for path lengths of 123 meters or greater; a shorter multiple-pass cell served for paths up to 28.84 meters. A custom-made grating monochromator employing a liquid-helium-cooled Ge:Cu detector was used to scan spectral curves of transmittance and to isolate very narrow spectral intervals for detailed study. Essentially all of the optical path outside of the sample cell was confined to two vacuum tanks to eliminate absorption by atmospheric gases. The only exception was a path of a few cm between the globar energy source and a window to one of the vacuum tanks. This short path was flushed with dry N₂. Polyethylene windows were used on the sample cells and on the vacuum tank where the energy beam entered from the globar source. The detector contained a KRS-5 window.

The grating used for the data in this section contains 45 lines/mm and is blazed at 22 µm. A long-pass interference filter eliminated overlapping orders of higher-wavenumber energy passed by the grating monochromator. Detector signals were processed with a synchronous demodulator and amplifyier, and the dc output of the amplifier was displayed on a strip-chart recorder. Transmittances were determined by dividing the signal output observed with the sample in place to that observed with the sample cell evacuated.

All sample pressures below approximately 0.08 atm were measured with an oil manometer; higher pressures were measured with an Hg manometer. Mixtures of $\rm H_20 + \rm N_2$ were formed by first adding the $\rm H_20$ to the evacuated sample cell and allowing the gas to stabilize before measuring its pressure. The $\rm N_2$ was then added slowly, allowing it to mix with the $\rm H_20$. Table 4 summarizes the important parameters of the samples for which detailed spectral data are presented. Absorption by several other samples not listed was investigated at certain wavenumbers of interest without scanning the spectra. The $\rm H_20$ partial pressure $\rm p$ and the total pressure $\rm P$ are given in the second and third columns; all samples were either pure $\rm H_20$ or $\rm H_20 + \rm N_2$. The absorber thickness u shown in the fifth column is expressed in molecules/cm² and is related to the other sample parameters by Eq. (1). The number associated with u has been abbreviated: for example, 169. +20 denotes 169 x $\rm 10^{20}$ molecules/cm².

The final three columns of Table 4 give the resolution schedule, the region over which spectra have been scanned, and the number of the figure in which the spectrum appears. Table 5 lists the spectral slitwidth corresponding to the resolution schedules given in Table 4. Spectral slitwidths given in Table 5 correspond to the full width at half-maximum of a triangular slit function.

RESULTS

Figures 4 through 9 shows the computer-plotted spectra for the samples represented in Table 4. The important sample parameters are repeated in each figure. The original recorder tracings have been smoothed somewhat during the digitizing process; thus the original noise level was higher than that indicated by the computer-plotted curves in Figures 4 through 9. The estimated errors in the plotted values of transmittance vary from less than 0.02 near 440 cm⁻¹ to 0.03 near 330 cm⁻¹. At points where T is near zero or near unity, the errors are probably lower.

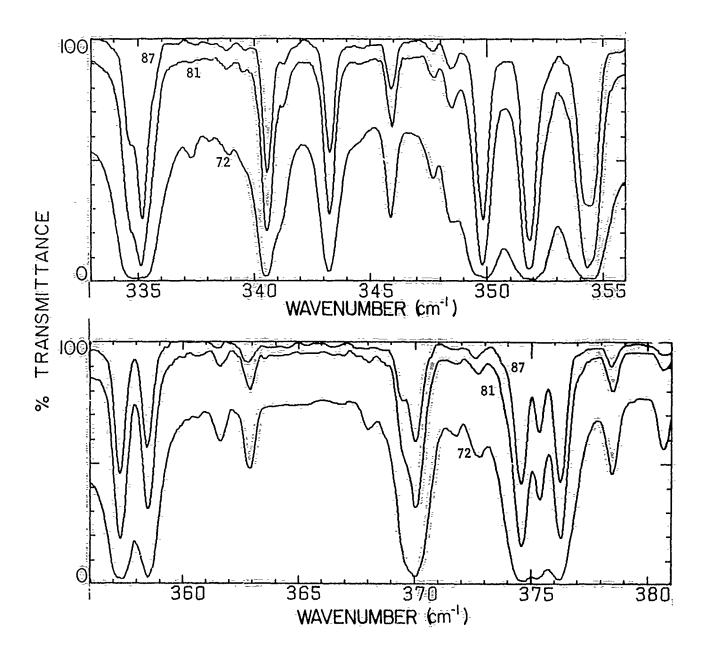
Tables 6 and 7 list values of the cumulative integrated absorptance based on the same samples as those represented by Figures 4 through 9. Each column corresponds to the sample indicated at the top.

TABLE 4. H₂O SAMPLE PARAMETERS

Sample No.	p (atm)	P (atm)	L (cm)	u :(#/cm ²)	(°K)	Res1. Schedule	Spectral Region (cm ⁻¹)	Figure No.
173	0.0115	0.0115	59500	169.+20	296	В	380-444	S
171	0.00882	0.00882	59500	130.+20	296	В	380-444	9
170	0.00553	0.00553	59500	81.6+20	296	В	380-444	9
61	0.0213	0.0213	2884	15.2+20	296	A	380-444	7
56	0.0158	0.0158	420	1.65+20	296	A	380-444	7
136	0.0207	1.004	2884	12,9+20	338	A	380-444	8
133	0.0207	0.500	2884	12,9+20	338	A	380-444	8
115	0.0208	ó.0208	2884	12.9+20	338	A	380-444	8
182	0.0141	0.0141	12300	43.0+20	296	С	333~381·	6
180	0.00868	0.00868	12300	26.5+20	296	Ğ	333-381	6
72	0.0207	0.0207	2884	14.8+20	296	Č	333-381	4
81	0.0211	0.0211	420	2.19+20	296	Ċ	333-381	4
87	0.0105	0.0105	420	1.09+20	296	C	333-381	4
111	0.0326	0.0326	2884	20.7+20	333	С	333 - 381	5
147	0.0212	1.000	420	1.93+20	338	Ğ	333-381	5
141	0.0213	0.500	420	1.95+20	338	Č	333-381	5
104	0.0213	0.0213	420	1.95+20	338	Č	333 - 381.	5

TABLE $\bar{\mathbf{5}}$. SPECTRAL RESOLUTION SCHEDULE

(cm ² 1)	(cm ⁻¹):	(cm ² -1)	(cm ⁻¹):
380	0.23:	0.32	0.42
3.90	0.25	0.34	0.46
400	0.28	0.36	0.48
410	0.30	0.39	0.52
420	0.32	0.42	0.56
43 <u>0</u>	0.35	0.45	0.60
440	0.37	0.48	0.64
450	0.39	0.51	0.68



Samp 1e	p≕P	u o
No	(atm)	(molecules/cm2)
8 7 -	0.0105	1.09×10^{20}
<u>8</u> 1:	0.0211	2.19×10^{20}
72	0.0207	14.8×10^{20}

Figure 4. Spectral curves of transmittance of H_2O from 333 to 381 cm⁻¹. θ = 296 K for all samples.

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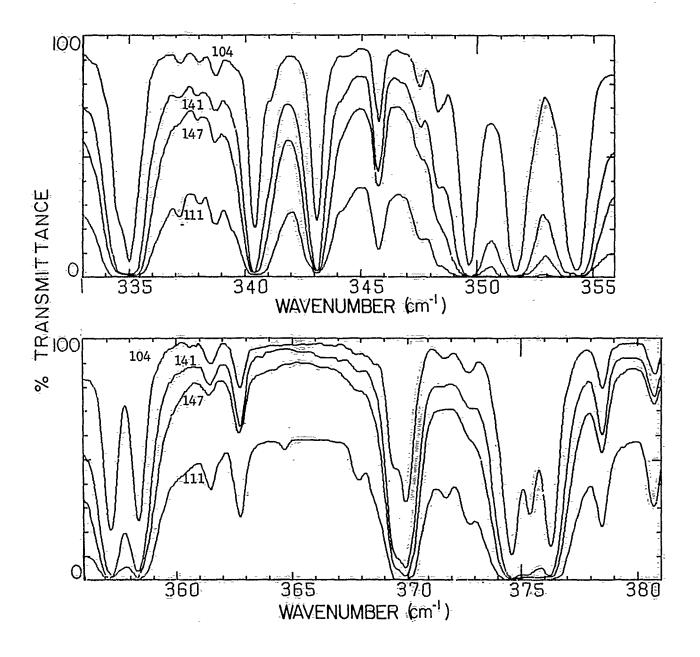


Figure 5. Spectral curves of transmittance of H_2^0 from 333 to 381 cm⁻¹.

Sample	p	P	u	θ
No	(atm)	<u>(atm)</u>	<u>(mõlecules/cm²)</u>	(°K)
104	0.0213	0.0213	$1.95 \times 10_{20}^{20}$	338
141	0.0213	0.500	1.95×10^{20}	338
1 47	0.0212	1.00	1.93×10^{20}	338
111	0.0326	0.0326	20.7×10^{20}	333

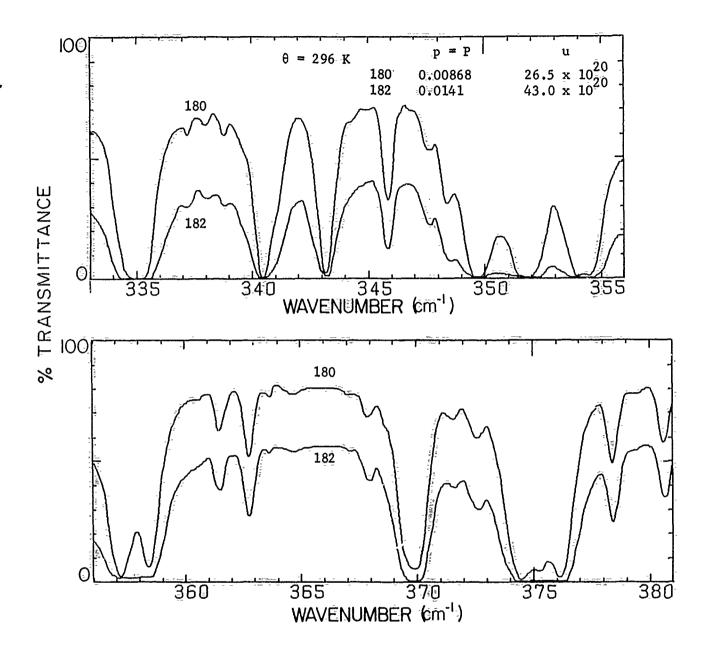
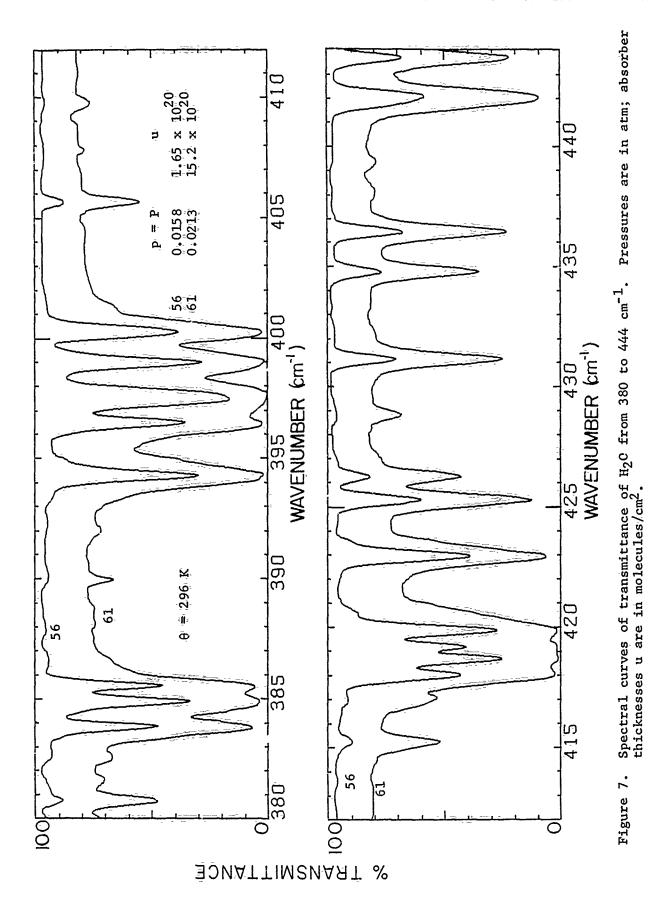
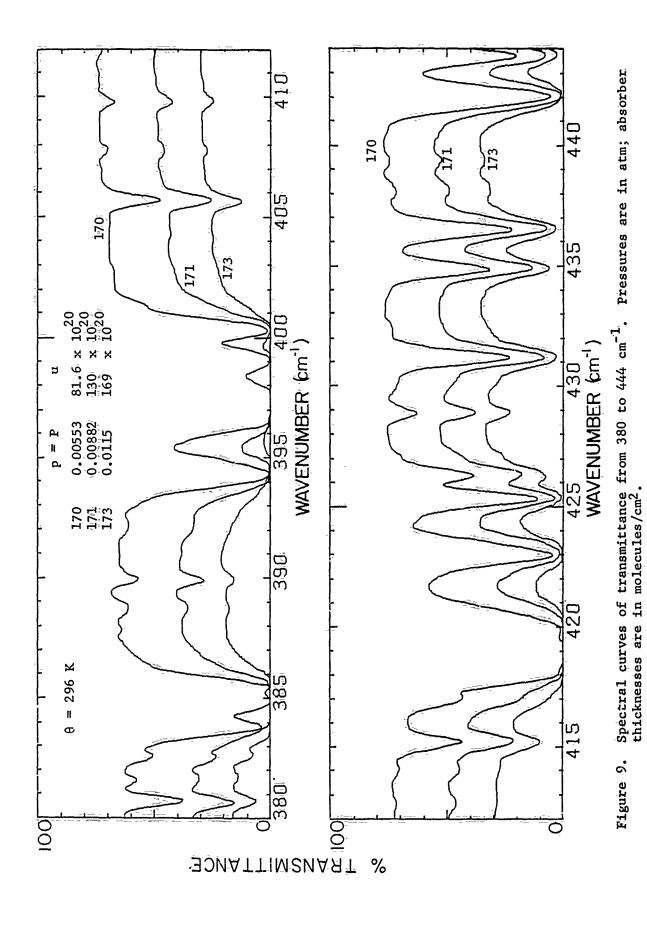


Figure 6. Spectral curves of transmittance of H20 from 333 to 381 cm⁻¹. Pressures are atm; absorber thicknesses u are in molecules/cm².



Spectral curves of transmittance of ${
m H_2O}$ from 380 to 444 cm⁻¹. Pressures are in atm. Figure 8.



	1											
	104- 336- 460- 0-02132 0-02132 1-945£ 20			9.28	44444444444444444444444444444444444444	9.5.25	100kg 1111kg 1111kg	4.543. 9.543. 9.545. 9.545. 9.645.	519.6 529.6 6.6 6.6 7.7 7.7 7.7 7.7 7.7 7.7 7.7 7	******		9.71.0 9.71.0 9.72.0 9.72.0
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TÁB	141- 336- 420- 0-02132 0-50000 1-945E 20	6979 9689 9290 6979 9879 6559 9279 4279 9870 9279 4279 9870	0.000 0.513 0.524 0.000 0.605 0.000 0.605 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000	1.993 1.565.3 1.993 1.566.1 1.993 1.566.2 1.993 1.566.5 1.993 1.566.5 1.993 1.566.5 1.993 1.566.5 1.993 1.566.5	2.781 2.427 2.155 2.965 2.578 2.268 3.137 2.786 2.346 3.299 2.416 2.414 3.453 2.988 2.473	3,690 2,990 2,524 3,745 3,667 2,524 3,695 3,61 2,625 5,635 3,724 2,625 6,163 3,274 2,716	5.763 5.407 5.407 5.407 5.407 5.407 5.405 5.405 5.406 5.406 5.406 5.406 5.406 5.406 5.406 5.406 5.406 5.406 5.406 5.407	0.00 to 0.00 t	999999 99999 99999 99999 99999 99999	5.157 4.247 5.325 4.385 5.478 4.581 5.599 4.581 5.698	5-79 6-718 5-866 6-769 5-862 6-818 6-876 6-917 6-876 5-987	# # # # # # # # # # # # # # # # # # #
πĀΒ̈́	111. 147. 141. 333. 338. 338. 338. 2684. 460. 460. 0.03284. 0.00218 0.00213 0.03284. 1.00000 0.50000 2.015E 21 1.933E 20 1.945E 20	58°9 95°9 92°0 58°9 92°1 55°9 92°9 52°1 98°°0 95°9 50°9 50°0 95°9 50°9 50°0	100 mm m	1.993 1.565.3 1.993 1.566.1 1.993 1.566.2 1.993 1.566.5 1.993 1.566.5 1.993 1.566.5 1.993 1.566.5 1.993 1.566.5	2.781 2.427 2.155 2.965 2.578 2.268 3.137 2.786 2.346 3.299 2.416 2.414 3.453 2.988 2.473	3,690 2,990 2,524 3,745 3,667 2,524 3,695 3,61 2,625 5,635 3,724 2,625 6,163 3,274 2,716	5.763 5.407 5.407 5.407 5.407 5.407 5.405 5.405 5.406 5.406 5.406 5.406 5.406 5.406 5.406 5.406 5.406 5.406 5.406 5.407	CONTROL OF THE PROPERTY OF THE	4.225 3.896. 4.391 3.526 4.379 5.669 4.775 5.894 4.8971	6.794 5.157 4.267 6.916 5.425 4.185 7.172 5.478 4.591 7.504 5.599 4.591 7.504 5.459	5-79 6-718 5-866 6-769 5-862 6-818 6-876 6-917 6-876 5-987	75 0 25 127 127 127 127 127 127 127 127 127 127
πĀΒ̈́	286. 233. 338. 238. 420. 420. 420. 420. 420. 420. 420. 420	6929 965 9290 580 000 000 000 000 000 000 000 000 00	150 0 150 0	\$19.2 165.2 569.0 \$49.1 569.0 \$49.1 569.0 \$49.1 139.1 166.7 2 \$49.1 129.1 166.7 2 \$40.1	\$15.5 \$1.	2.523 2.524 2.525	5.763 5.407 5.407 5.407 5.407 5.407 5.405 5.405 5.406 5.406 5.406 5.406 5.406 5.406 5.406 5.406 5.406 5.406 5.406 5.407	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	5-816 4-225 3.333. 5-816 4-391 3.523 6-39 4-577 3.894 6-597 4-775 3.894 6-597 4-871	6.794 5.157 4.267 6.916 5.425 4.185 7.172 5.478 4.591 7.504 5.599 4.591 7.504 5.459		69-69-6-537 55.1.46 6-6-69-6-537 55.1.71 6-6-69-6-597 55.1.71 6-6-69-6-69-69-69-69-69-69-69-69-69-69-6
ΤÂΒ̈́	254. 254. 333. 338. 338. 254. 260. 260. 0.02103 0.0228	6229 9629 9299 6599 6629 6599 6529 6529	125 0 125 0	\$11.2 152.2 165.2 559.0 91.1 150.1 1	1.15	1553 1551 1551 1551 1551 1551 1551 1551	2.757					
πÄ́B	12. 81. 87. 111. 147. 141	6279 9679 9290 5888 1888 9170 6670 6670 6670 6670 6670 6670 6670 6	10.755 18.110 0.612 18.606 1.5513 18.574-10.013 18.674-10.013 18.675-10.	\$11.2 152.2 165.2 559.0 91.1 150.1 1	\$51.5	1,515 1,517 1,517 1,518	1,556 1,757 1,501 5,130 5,755 1,500					
ΤÂΒ̈́	254. 254. 333. 338. 338. 254. 260. 260. 0.02103 0.0228	6279 96579 92970 58070 EEFE 91770 56574 18770 96574 18	0.459 0.555 0.130 0.482 0.100 0.513 0.374 0.455 0.45	\$1192 1522 16522 16540 9150 5641 1781 1781 1781 1781 1781 1781 1781 17	\$255 525 75.0 5.0 6.75 6.75 6.75 5.55 5.55 5.55 5.55 5.55	2-717 2-195 1-554 1-554 1-554 1-554 1-554 1-555	3.451 3.484 1.556 8.757 0.381 3.30 2.753 3.453 3.454 1.653 8.765 0.565 1.653 3.467 2.553 3.259 3.455 1.659 8.755 1.558 2.558 3.359 3.455 1.659 8.775 1.558 2.558	1,130 1,142 1,1435 1,1435 1,143 1,14				

9.77 4.75 9.77 9.16 9.16	9.972 9.972 10.093 11.163	2755- 275- 275- 275- 275- 275- 275- 275-		18.787 10.726 11.726 11.736 10.759	1999	11.259 11.259 11.259 11.551 11	11: 727 11: 955 12: 955 12: 24	12.55 12.55	12.000 13.015 15.000 15.000 15.000			200 200 200 200 200 200 200 200 200 200
17.56 17.51 17.51 17.51 17.57 18.61	17.672 17.753 17.965 10.196	0,000 0 0,000 0,000 0,000 0,000 0,000 0,000 0 0,000 0 0 0 0 0 0 0 0 0 0	2447 6447 6447 6447 6447 6447 6447 6447	11 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	19.51 19.61 19.61 19.757 19.85	26.814 26.375 26.375 28.973 28.973	200 1 1 1 2 1 2 1 2 1 2 1 2 1 2 1 2 1 2	9 19 19 9 8 19 19 9 7 10 10 2 10 2	55.44 52.54 54.65 54.65 53.64 54.64	21.15 21.15	**************************************	23.637
23.664 23.664 23.119 21.119	21.272 21.392 21.591 31.737	22.126 22.513 22.513 22.513 22.566 22.566	24.67 26.67 26.67 26.67 26.67 26.67 26.67 26.67 26.67 26.67 26.67 26.67	**************************************	25.45 25.45 27.45 27.65	25.11 27.11 27.51 27.51 27.51 27.51 27.51	22222 22222	26.155 26.55 26.55 26.55 26.55 26.55 26.55 26.55	27-02 27-02	27.522	44.44	28.844 26.864 26.894 28.154 28.154
27.05.0 27.05.	422.62 52.62 52.62 52.62 52.62	29.62. 29.62. 29.821 39.921	00000000000000000000000000000000000000	2000 N N N N N N N N N N N N N N N N N N	31.666	162621 62621 62621 8627 8627 8627 8627 8627 8627 8627 8627	11.72.9 11.72.9 11.72.9 11.72.9 11.72.9	26-52 52-72 52 52-72 52-72 52-72 52-72 52-72 52-72 52-72 52-72 52-72 52-72 52-72 52-72 52-72 52-72 52-72 52-72 52-72 52-72 52-72 52-	**************************************	100 100 100 100 100 100 100 100 100 100	# 2 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	10. 10. 10. 10. 10. 10. 10. 10. 10. 10.
1925	11221	**************************************	\$60000 \$600000 \$600000 \$600000 \$600000 \$600000 \$600000 \$600000 \$600000 \$6000000 \$600000 \$600000 \$600000 \$600000 \$600000 \$6000000 \$6000000 \$600000 \$600000 \$60000000 \$6000000 \$6000000 \$600000000	8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	25.55 11.55	**************************************	*****	# # # # # # # # # # # # # # # # # # #	6.25 6.25 6.25 6.25 6.25 6.25	6.264 6.389 6.389		######################################
7,000 M 100	4.55 4.55 4.55 4.55 4.55 4.55 4.55 4.55	9.979 10.119 10.219 10.279 10.000		12++51 10++35 10++35 10++35 10++35	10.522 10.941 10.941 10.941	10 - 667 10 - 490 11 - 690 11 - 226	11.455	185°21 882°21 602°21	616-71 15-54 15-71 15-71	12.651	25.55 25.55	12.716 12.735 12.735 12.735
21.518 21.554 21.657 21.657 21.726 21.726	21.00 22.00 22.00 22.00 22.00 22.00 22.00 20 20 20 20 20 20 20 20 20 20 20 20 2	\$6.25 \$6.25 \$6.25 \$6.25 \$6.25 \$7.25	23.44 23.53 23.63	21.93 21.93	54° 588 54° 385 54° 436 54° 688 54° 688	24.911 25.991 25.101 25.378 25.578	29-771 25-9-66- 26-146- 26-148- 26-148-	26.783 26.929 27.124 27.388 27.469	27.60 27.60 27.60 27.90 27.90 27.90	\$6.5.85 \$6.6.85 \$6.2.85 \$6.2.85 \$6.2.85	200 00 00 00 00 00 00 00 00 00 00 00 00	28.45 28.745 28.691 29.878 26.965
19.582 19.582 19.613 19.613		\$5157 \$8.57 \$8.57 \$8.57	20222	21.63 21.761 21.039 21.039	21.996 22.152 22.152 32.253	22.52 22.490 22.490 23.490 23.294	23.55 23.55 23.55 23.55 25.55	\$11000 \$1000	22:52 23:52 23:52 23:53	22222 22222	*****	26.19 26.23
27.885 27.199 27.587 27.5421 27.547	27.607 27.944 28.038 28.228 28.228	72 1 6 7 7 2 1 6 7 7 2 1 6 7 7 2 1 6 7 7 2 7 6 7	126 - 62 146 - 62 150 - 62 150 - 62 150 - 62 150 - 62	5 ~ 4 6 6 6 ~ 4 6 6 6 ~ 6 7 7 7 8 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	2000 2000 2000 2000 2000 2000 2000 200	# # # # # # # # # # # # # # # # # # #	**************************************	\$2.6° 88 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	1100 A A A A A A A A A A A A A A A A A A	54.54.54.54.54.54.54.54.54.54.54.54.54.5	500 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	200 200 200 200 200 200 200 200 200 200
90 - 0 - 0 - 0 - 0 - 0 - 0 - 0 - 0 - 0 -	**************************************	170.00 170.00 170.00 170.60 170.60		372.00 372.46 372.46 372.66	373, 20 373, 20 373, 48 373, 48 373, 66	376.08 376.28 376.28 376.48	25 kg 27 kg 28 kg	376. 18 376. 18 376. 18 376. 18	64 - 14 - 14 - 14 - 14 - 14 - 14 - 14 -	00000000000000000000000000000000000000	**************************************	200 - 200 -
	3.226 3.226 3.265 3.065	N6343	27464	2.625	0,000 0 0,000 0,000 0,000 0,000 0,000 0,000 0,000 0 0,000 0 0,000 0 0 0		*****		******	:::::: :::::::::::::::::::::::::::::::	5235	74.96.9 74.96.9 74.96.9 74.96.9
		-	-	**************************************								
N = 11 + 1 + 1 + 1 + 1 + 1 + 1 + 1 + 1 +	6.176 6.211 6.293 6.376	56555 56555 56555 56555	THE HE H		7.621 7.77 7.962 8.196 8.156	6.552 8.759 9.919 9.291	######################################		11.927 11.672 11.693 11.611	\$6.521 1.2.399 1.2.35 1.2.55 1	5 0 0 0 0 0 5 0 0 0 0 0 5 0 0 0 0 5 0 0 0 0	12.0 03.0 12.0 03.0 12.0 03.0 12.0 03.0 13.0 03.0 03.0 13.0 03.0 1
N = 11 + 1 + 1 + 1 + 1 + 1 + 1 + 1 + 1 +	7.566 6.176 7.727 6.211 7.79 6.246 7.861 6.293 7.968 6.376	6.803 6.191 6.191 6.192 6.193 6.196 6.693 6.196 6.196 6.196	HARMS OF STREET	222777	7.621 7.77 7.962 8.196 8.156	18.599 0.552 10.799 0.750 10.996 0.960 11.131 9.119 11.303 9.219	11.577 9.464 11.776 9.464 11.776 9.844 12.176 18.839	12.575' 18.447 12.773' 18.655' 12.971 18.626' 13.167 11.626 18.059 11.177	13,546 11,327 13,729 11,676 13,919 11,634 16,106 11,634 16,107 11,991	16 - 561 12 - 192 16 - 761 17 - 192 17 - 193 17 17 17 17 17 17 17 17 17 17 17 17 17	15 - 6 - 6 - 13 - 13 - 13 - 13 - 13 - 13 -	12.0 03.0 12.0 03.0 12.0 03.0 12.0 03.0 13.0 03.0 03.0 13.0 03.0 1
5.50 5.50 5.72 5.50 5.72 5.50 5.50 5.50 5.50 5.50 5.50 5.50 5.5	7.666 6.176 7.727 6.211 7.79 6.246 7.861 6.293 7.968 6.376	10.654 11.165 11	11,566) 6,467 11,702: 0,516 12,646; 0,557 12,646; 0,557 12,646; 0,577 12,647 12,647 12,647 12,647 12,647	6.812 7.813 6.999 7.124 9.139 7.234 9.293 7.486 9.659 7.466	13.279 5.626 7.621 11.476 9.616 7.776 13.676 10.601 7.796 13.676 10.401 6.195 16.676 10.401 6.195	10,276 11,219 12,520 12	15.276 11.577 9.446 15.476 11.376 9.446 15.476 11.376 9.446 15.476 12.376 11.486 14.476 12.376 11.236	16.276 12.575 18.637 16.776 12.773 16.635 16.6476 12.471 18.628 16.676 13.467 11.638 17.875, 18.359 11.177	17.273 13.546 11.127 17.671 13.729 11.676 17.671 13.915 11.638 17.671 16.116 11.631	### ##################################	15 - 6 - 6 - 13 - 13 - 13 - 13 - 13 - 13 -	25.2010 16.316 13.638 21.312 15.521 15.927 21.312 15.521 15.322 21.312 15.321 15.322 21.312 15.311 15.277
5.50 5.50 5.72 5.50 5.72 5.50 5.50 5.50 5.50 5.50 5.50 5.50 5.5			11.556 11.556 11.556 11.556 11.556 11.556 11.556 11.556 11.556 11.556 11.556 11.556 11.556 11.556 11.556 11.556	12.145 6.612 7.639 12.716 9.139 7.234 12.831 9.139 7.234 13.663 9.139 7.466						10.21 10.21		
3.134 1.484 1.426 7.243 5.487 1.135 1.487			1010 1210 1210 1210 1210 1210 1210 1210			255		200 100 100 100 100 100 100 100 100 100		1.552 1.500 1.571 1.571 1.521	7.03	
3.134 1.484 1.426 7.243 5.487 1.135 1.487		1000 1000 1000 1000 1000 1000 1000 100	1019 1019 1019 1019 1019 1019 1019 1019	1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00		250	100 100 100 100 100 100 100 100 100 100	71.01 (1.02.	13.550 6.111 1.125 17.272 13.54 11.277 11.27	15.25	7.03	
7.231 3,136 1,496 1,426 7,224 5,497 7,332 7,332 1,496 1,496 1,426 7,347 5,498 7,347 5,498 7,347 5,498 7,498		7-216	7.57.0 6.59.0 1.55.7 1.56.7 1.55.6 1.55.6 1.57.7 1.57.7 1.57.6 1.57.7 1.	1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00		255 11.51 12.52 12.51 15	100 100 100 100 100 100 100 100 100 100	11.05 12.00 2.00 2.00 10	13.550 6.111 1.125 17.272 13.54 11.277 11.27	10.77 10.27		

TABLE 7 $\int_{\nu}^{A} d\nu$

Sam. Fo. Temp (K) Path (cm) p. (atm)	173. 296. 59500. 0.01145 0.01145	171 • 294 • 59500 • 0 • 00682 0 • 00882	170+ 294+ 59500- 0-00553- 0-00553-	61. 296. 2884. 0.02132 0.02132	56. 296. 420. 0.01579 0.01579	134. 334. 2684. 0.02044 1.00395	133• _336• =2884• 0•02066 0•50000	115. 336. 2664. 0.02079 0.02079
P (atm) u=(#/cm²)*	1.670E 22	1.301E-22 8	-158E-R1 1	525E 21	1.645E 20			3035 51
(c <u>m</u>)-1						-	•.	••
360.00 360.20 360.40 360.60 360.60	6. 8.168 8.338 9.519 8.786	0.134 0.276 0.435 0.602	0. 0.075 0.156- 0.261 0.384	0.052 0.133 0.177 0.279	8.807 8.813 8.826 8.848	1.138 1.269 1.424 1.597	8.898 0.192 0.326 0.481	0.043 0.048 0.159 0.265
391.60 361.20 361.40 361.60 391.80	8.888 1.059 1.228 1.398 1.571	8.756 0.891 1.025 1.163 1.302	0.494 8.575 7.652 0.736 8.818	0.369 0.426 8.481 0.539 3.597	0.066 8.880 - 8.891 8.191 8.188	8.760- 8.904 1.840 1.175 1.309	8.605 0.706 -0.759 0.334 0.987	8.352 8.483 8.455 0.509 0.563
382.00 382.20 382.50 382.50	L.741 1.918 2.84 2.266 2.450	1.437 1.572 1.717 1.869- 2.020	0.894 0.971 1.857 1.154 1.251	6.649 6.768 8.768 6.825 0.890	0.114 0.119 0.128 0.141 0.156	1.445 1.582 1.727 1.878 2.038	1.075 1.166 1.272 1.357	0.609 8.653 0.710 0.778 8.838
362.80 -363.06 393.20 393.48 363.60	2.633 2.822 3.016 3.217	2.174 2.336 2.588 2.691 2.884	1.345 1.449 1.577 1.739 1.927	8.952 1.824 1.138 1.272 1.451	0.170- 0.193 0.202 0.236 0.316	2.207 2.390 -2.584 2.784 2.984	1.641 1.791 1.966 2.158 2.356	0.895 0.963 1.059 1.203 1.380
383.80 -384.80 384.20 384.40 384.60	3.617 3.617 3.617 6.817 6.217	3.682 3.282 3.482 3.682	2,117 2,293 2,465 2,649	1.638 1.782 1.922 2.889	0.411 8.451 8.481 8.527	3.184- 3.304- 3.564 3.784 3.994	2.556 2.756 2.756 3.156 3.156	1.559 1.712 1.851 2.015 2.200
334.80 395.80 385.20 385.40 385.60	6.617 6.617 6.817 5.017 5.217	3.882 4.882 4.282 4.482 4.682	2.846 3.845 3.243 3.439 3.637	2.277 2.469 2.654 2.437 3.824	8.618 8.744 8.828 8.878 8.981	-6.194 6.384 6.584 6.794	3,556 .3,754 -3,951 4,147	2.392 2.567 2.736 2.913 3.071
385.80 386.00 386.20 386.40	5.417 5.615 5.808 5.994	4.879 5.867 5.239 5.348 5.549	3, <u>8</u> 16 3,966 4,882 4,181, 4,272	3.192 3.388 3.394 8.469 3.537	1.854 1.877 1.887 1.893 1.110	5.183 5.374 5.553 5.718	4,539 4,517 4,674 -4,011 4,6938	3.178 3.249 3.307 3.358
396-60 366-90 -387-00	6.174 6.348 6.519	5.692 5.438	4.857-	-3.599 3.655	1.132	5.872 6.017 6.154	5.034 5.129 5.219	3.485 3.449 3.491
387.20 397.40 387.60 387.80	6.686 6.852 7.015 7.177	5.964 6.095 6.222 6.346	4.514 4.518 4.657 4.728	8.767 3.758 3.488 3.458	1.140 1.146 1.152 1.161	6.283 6.405 6.522	5.305 5.367 5.465	3.581 3.569 3.606
365.00 365.20 365.40 366.60	7.339 7.501 7.663 7.827	6.471 6.595 6.720 6.847	4,808- 4,878= 4,941- 5,017-	5.907 3.959 4.010 4.061	1.171 1.160 1.169 1.196	6.635 6.746 6.856 5.966	5.543 5.620 5.695 5.769	3.642 3.678 3.715 3.754 3.798
388.80 389.00 389.20	7.992 3.156 3.313	6.976 7.104 7.228	5,096 5,172 5,241	4.161 4.288	1.203 1.210 1.216	7.077 7.189 7.296	5.847 5.926 6.005 6.001	3.848 3.879 3.911
369.60 369.60 369.60	9.460 9.643 9.609	7.548 7.468 7.600	5,305 5,370 5,446	4.253 4.299 4.348	1.228	7.511-7.636	6.158 6.250	3,945 3,989 4,858
390,00 390,20 390,60 390,60 390,80	8.977 9.143 9.305 9.463 9.620	7.742 7.875 7.999 4.121 8.243	5,531 5,612 5,606 5,756 5,827	4.412 4.467 4.514 4.568 4.685	1.248 1.260 1.271 1.282 1.291		6.361 6.455 6.533 6.649 6.685	4.108 4.142 4.184 4.225
391.09 391.20 391.60 391.60 391.60	9.776 9.938 18.898 18.259	8.498 8.614 8.739	5.497 5.967- 6.037 6.107: 6.188-	-4.650 4.695 4.741 4.789	1.317 1.326	8.466 8.581 8.781	-6.759 6.633 -5.987 6.987 7.079	4.264 4.302 4.339 4.379 4.425
392.80 392.20 392.48 392.68	18.508 10.754 18.923 11.893	8.999 9.133 9.267 9.482	6.257 6.336 6.413 6.485	4.896 4.952 5.005 5.056 5.109	1.354 1.366 1.377	9.095 9.235 9.381	7.168 7.281 -7.377 7.479 7.588	4.477 4.526 4.570 4.616 4.665
392.80 393.00 393.20 393.60	11.266 11.443 11.623 11.809	9.678 9.625 9.943	6.566 6.737- 6.836 6.951-	5.169 5.226 5.393 5.391	1.396 1.406 1.422 1.436	9.768 9.873 10.857 18.258	7.710 7.847 8.003 8.175	4.718 -4.778 4.851 4.942 5.859
393.80 394.80 394.20 394.40	12.190 12.305 12.562 12.762	10.335 10.529 10.727 2- 10.526	7,095 7,266 7,458 7,656	5.586 5.664 5.853 6.849	1.500 1.600 1.734	18.645 18.645 11.035	8.561 8.768 8.959	5.223 5.416 5.603 5.709
394.60 394.60 395.80	12.982 13.182 13.382	2 11.324 2 11.517	4.4 <u>2</u> 7 4.146	6.34	1.469 3 1.89	11.644	9,356	5.947 6.092 6.193
395.20 395.40 395.60 395.80	13.591 13.770 13.970 14.16	11.781 6 11.677 0 12.053 6 12.234	8.563 8.692	6.70 6.79 6.89	1.93 3 1.94 2 1.96	12.044	9.924	6.242 6.369 6.462

		Т	ABLE	7	(cont d)		
Sam. No. Temp (K)	173• 2961	171• 276•	170 · 296 ·	61 · 276 ·	34.=	134 • 338 •	133.	115.
Path (cm) p (atm)	57500+ -0.03145	59500+ 0+00882	59500+ 0-00553	2884. 0-02132	420-	2554. 0.02066	2884. 0.02046	0.02079
P. (atm),	0.01145	0.00582	0.00553	0.02132 .525E 21	0.01579	1.00395 1.2946 21 1	0.50000	0.02079 .303E 21
(œ)-1					1			
	14.359	12.422	1.436	7.012	1.981	12.644	18.486	6.573
396.20	14.556	12.614	9.005 9.196	7.174 7.364	2.119	12.844	10.68Z 10.361	6.723
396.40 396.60	16.953	13.415 13.215	9.395	7.557 7.743	2,243	13.244	11.980 11.280	7.181 7.289
396. 40 397. 40	15.353	13,415	9.794	7.930	2,376	13.644	11.486	7.474
397, 20 397, 40	15.553 15.753	13,615	9,994	8.123- 8.328	2,463.	13.844 14.844	11.680 11.880	7.666 7.862
397.60 397.60	15.953 16.153	14.015	10.394 18.594	6.519- 6.717	2.775	16.246 16.666	12.200	8.859 8.255
395.00	16.353	14.415	10.790	4.907	3.029	14.644	12.4 06 12.680	8.447 8.621
395.20	16.553 16.753	14.615	10.977	9.075 9.224	3.102	16.844	12.888 13.080	6.782
398.60 -395.80	16.953 17.153	15.015 15.215	11.339 11.529	9.383 9.566	3.202	15.244 15.444	13.266	9.131
399.00	17.353	15.415	11.726	3.761 9.955	3,331	15.644 15.844	13.488 13.679	9.327 9.528
399.20 399.40	17.553	15.615 15.814	11.925	18.126 18.270	3,584	16.044	13.678	9.740
399.60 399.80	-17.952 13.151	16.009 16.203	12.295 12.456	10.397	3,555	16.444	14,273	9.967
400.00	13.350	16.399 16.597	12.623 12.512	10.554 10.742	3,596	16.644	14.470 14.669	10.142 10.327
400.20	13.550 18.750 13.949	16.796 16.995	13.008	10.935	32017	17.844	14.864 15.066	18.521 10.701
400.60 400.50	19.145	17.187	13.359	11.229	3-931	17-444	15.259	10.544
401.00 401.20	19.335	17.361 17.524	13,4 83 13,584	11.322 11.394	3.946	17.648	15.438 15.682	10.941
401.40 401.60	19.697 19.869	17.676 17.828	13.676	11.463 11.526	3.978 3.961	18.011 15.179	15.752 15.442	11.058
401.30-	24.036	17.556	13.637	11,580	3.991	18.332	15.997	11.194
402.00	23.195 23.357	19.043 18.206	13.904	11.638	4.800 4.008 6.816	18.474	16.098- 16.191	11.233
402.40	28.515 28.671	18.327 18.446	14.036 14.191	11.726	67022	18.658	16.276 16.363	11.337 11.343 11.378
402.50	28.826	13.564	14,167	11.517	4.036	18.963	16.442	11.412
403.00 403.20	28.980 21.132	18.681	14,231	11.861	4.443	19.073	16.589 16.658	11.445
403.40 403.60	21.234 21.434	18.909 19.022	14,355	11.947	4.057	19.279	16.726 16.791	11.511 -11.545
403.30	21.584	19.134	14.478	12.032	-4.072	13.471	16.355	11.578
404.80 404.20	21.734	19.246 19.359	14.539 14.688 14.662	12.116	4.074	19.657	16.919 16.983	11.615-
404.60	22.035	19.474 19.585 19.701	14.724	12.205 12.247	4.891	19.838	17.044 17.102	11.693 11.726
404.50	22,333 22,493	19.514	14.848	12.267	4.105	28.015	17.160	11.757
405.00 405.20	22.635 22.791	19.927	14.918	12.328	4.112 4.120	28.105 28.269	17.220	11.788 11.825
405.40 405.60	22.961	20.136	15.860 15.172	12.450 12.536	-4.149 -4.164	28.347	17.406 17.539	11.887 11.966
405.80 406.00-	23.295	20.471	15.256	12.594	4.177	28.626	17.637	12.016
406.20 406.40	23.592	20.568	15.324 15.382	12.637 12.678	4.184	28.719 28.800	17.708 17.752	12.149
406.60 406.50	23.736	20.885 20.912	15.434	12.718 12.759	4.196 4.288	28.675	17.962 17.851	12.110 12.148
407.00	26.82"	21.017	15.547	12.799	4.210	21.029	17.898	12.168 12.196
407.20 407.40	24.105	21.171	15.691- 15.654	12.636	4.217		17.946 17.992	12.225
407.60	24.45 8 24.596	21.331 21.440	15.711 15.771	12.912 12.953	4.234 4.243	21.245	13.040 18.091	12.286
405.00	24.740	21.549	15.430	12.395 13.835		21.387	18.143 18.144	12.319 12.347
403.20 403.40	26.552 23.623	21.655 21.758	15.934	13.071 -13.108	4.267	21.525	18.242	12.374
408. EO 403. BC	25.164 25.306	21.962 21.965	15.998 16.044	13.145				12.428
409.00	25.447 25.597	22.069 22.172	16.097 16.158	18.182 13.254			19.364 18.430	12.454
409.20	23.728	22.274	16.204 16.261	13.247	4.298	-21.865	18.476	12.535 12.533
40 % 60 409 • 50	25.872 26.821	22.386	16.325	13.335	4,315	22.028	15.594	12.576
410.00 410.20	25-171 25-316	22.608 22.716	16.308	13.380	-4.332	22.157	16.715	12.623 12.656
410:40 410:60	26.459 26.601	22.820 22.922	16.496 16.549	15.454 13.491	47339	22.324	18.603	12.634
410.50	26.743		16,601	13.529	4.354	22.392	18-947	12.739
411.00 411.20	26.683 27.82 3	23.125 23.226	16.654	13.56 13.60	4,376	22.525	18.936	
411:40 411:60-	27.162 27.302	23.325 23.425	16.898		4:349	22.663	19.028	12.546
411.50	27.441	23.525	16.461	13.71		22.733	19.076	14.016

TABLE 7 (cont'd)

Sam. No. Temp (K) Path (cm) p (atm) P (atm) u (#/cm²)	173+ 296+ 59500+ 0+01145 0+01145 1+690E-82	171 · 296 · 59500 · 0 · 00662 0 · 00662 1 · 301£ 22	170+ 294+ 59500+ 0+00553 0+00553 5+158E 21	61 • 296 • 2884 • 0 • 02132 0 • 02132 1 • 525E 21	56. 296. 420. 0.01579 0.01579	136+ 336+ 2684+ ' 0+02066 1+00395 1+294E 21	0.0P066 0.50000	115- 336- 884- 0-02079 0-02079
							~ ~ -	
(cm) ⁻¹								
412.00	27 .5 62	28.626	16.917	13.752 13.790	\$.480 \$.407	22.885 22.879	19.124	12.494
412.28 412.48	27.723 27.866	25.833	16.972 -17.828	13.838	4.415	22.955	19.223	12.954
412.60 412.80	28.869 28.153	28.940 24.849	17.845 17.142	15.069 13.909	4.423	23.034	19.277 19.331	12.986 1 3.828
413.00	28.296	24.156	17-197	13.948	4.436	23.194	19.3.02	13.050
413.20 413.40	28.439	24.259 24.362	17.251 17.305	13.987 14.826	4.442	23.272 23.358	19.433 19.486	13.000 13.111
413.60	28.725	24.464	17.359	14.864	4.457	23.430 23.513	19.544 19.599	13.142 13.174
413.80	59.969	24.570	17.416	14.101			-	13.207
414.80 414.20	29.014 23.168-	24.680 24.791	17.475 17.535	14.139 14.174	4.473	23.599 23.68 6	19.656 19.717	15.241
414.40 414.60	29.347 29.455	24.901 25.013	17.592 17.653	14.219 14.2 6 2	4.487	23.700	19.788 19.847	-13.274- -13.308
414.60	29.611	25.131	17.723	14. 309	4.505	28.991	-19.924-	13,344
415.00	29 1770	25.267	17.813	14.375	4.517	26.125	20.029- 20.159-	13.410 13.492
415.20 415.40	29.956- 38.133-	25.419 25.575	17.919 18.826	14.462 14.553	4.535	24.434	28.295	13.5 00
415.60 415.80	31.299	25.715 25.839	16.109	14.616 14.665	4.571 4.581	24.577 25.709	20.412- 20.506	-13.638 13.678
		-	10.247	14.712	4.591	24.643	20.558	13.728
416.00 416.20	38.615	25.958 26.078	18.314	14.760	4.602	24.983	20.695	13.760 13.802
416.40 416.60	3 4.936 31.105	26.2 43 26.335	18.384 18.463	14.818 14.869	4.613	25.131 25.288	20.917	13.852
416. 80	27 -5 93	26.482	18,559	14.945	4.640	25.457	21.653	13.923
417.00	31.469	26.643	18.669	15. 83 4 15.127	4.675	25.639 25.829	21.286 21.372	14.609 14.896
417.20 417.40	31 .655 31 .655	26.889 26.988	18.783	15.216	4.692	26.024	21.551	14.183
417.60 417.80	32.049 32.249	27.162 27.351	19.839 19.206	15.327 15.478	4.714 4.767-	26.222	21,739 21,985	14.297 14.450
418.00	32.448	27.548	19.397	15.666	4.467	26.621	22.133	14.636
41 8. ZQ	32.648	27.748	19.593 19.791	15.061 16.053	4.974 5.855	26.821	22.332	14.829 15.022
415.40 418.6 ₂	32.646	27.948 28.148	19.991	16.248	5+170-	27.221	22.732	15.218
418.83	33.548	28.348	20.191	16.446	5.316.	27.421	22.932	15.415
419.00 419.20	33.44 6 33.64 8	28.54 8 28.748	20.591 20.591	16.642 16.839	5.424- 5.532	27.621	23.132 25.332	15.611 15.888
419.40	33.648	26.948	28.798	17.834	5.636 5.707	28.821	23.532 -23.732	16.003 16.196
419.60 419.80	36.048 36.24 8	29.148 29.348	20.987 21.185	17.422	5.020	28.421	23.931	16,389
420.00	-3. i 448-	29.548	21.342	17.617	5.961	28.621	247130	16,546
420.2) 420.40	34.648- 34.847	29.747 29.946	21.575	17.7 9 9 17.955	6.056 ⁻ 6.068	28.821	24.527 24.524 ×	16.768
420.70	36.18.46	30.141	21.919	18.891	6.115	29.221	24.719 24.989	17.046 17.161
420 : 80	35.243	30.330	•		6.155	29.616	25.049	17.256
421.00 421.20	35.435 35.621	36.587 30.673	22.191 22.298	18.383 -18.386	6.165=	29.807	25.256	17.326
421.40 421.60	35.601 35.977	30.826 38.972	22 ,398 22,47 6	18.446	6.176 5.186	29.994	25.412 25.5 66	17.389
421.88	36.154	31,115	22.561	18.575	6.195	i .	25,744	17.501
422.00	36.332	31.261	22.650	18.643	6.205	74.541	25 : 859 26 : 819	17.567 17.688
422.20 422.40	36.513 36.699	31.413 31.572	22,74 5 22,451	18.715 18.797	6.217	2 224	26.191-	17.719
422.60	36:893 37:891	31.744 31.932	22.981 23.144	18.989 19.866	6.873 6.873	31	.26:379 76:575	17.833
423.00	37.290	32.128	23.331	19.252	6	31.519	26.773	18.178
423.20	37:469	32.325 32.517	23.515 23.679	19.422	6,5,4-	31.714	26.971 27-166	18.358
423.40 423.60	37:647 37:641	32.766	23.416	19.668	6.604-	32.114	27,353	18.626
423.80	31 : 1,64	32.365	~23.927	19.739	6.622	32.302	27.518	
4 24.8 8 524.20	38.237	33.011 33.143	24.815 24.888	19.798 19.853-	6.631 6.639	32.480	27.663 27.793	18.774
424.40	38.568	33.271 33.461	24,161 24,238	19.988	6.644	32.815	27.919 28.050	16.876 16.928
424.60 424.88	38.732	33.536	24.325	20.630	6.661	38.165	28.196	18.992
425.00	39 : 0 54	33.645	24.439	20 - 129	6.691	33.355	26.3(5	19.891
425.20 425.40	397276 397474	33.873 34.863	24.592 24.7 68	28.276	6.749	38.552 33.750	26.561	19.237
425.68 425.88	39.678 39.859	34.251 34.422	24.929 25.849	20.566- 26.675-		33.949	28.958 29.125	19.573 19.676
				20.747	-6.914	34.325	29:200	19.746
426.88	487839	34.577 34.734	25.149 25.260	28.844	-6.942	36.506	29.437	19.027
426.48 426.68	48;446 48 <u>;</u> 543	34.617 35.654	25.341 25.466	20.955 21.040	6.976	34.692		20.013
426.60	48.745	35.147	25.564	21.693	7.886	34.988	29.849	28.849
427.00	41 . 8 9 8	35.385	25.630	21.141	7.816 7.825	35.200	29.929	20.688 20.123
427,28- 427,48-	41.846	35.416 35.525	25.698 25.745	21.186	7.832	35.298	34 . 4 43	. 28.154 20.161
427.68 427.88	41.460 41.460	35.624 35.728	25.797 25.847	21.266 21.303	7.037 7.042		30 : 1 21 30 : 1 76	20.207
	ofiu.are mole					•		

		Ī	BLE	7 (cont ¹ d)			
Sam. No. Temp (K) Path (cm) p (atm) P (atm) u (#/cm²)	173+ 296+ 59500+ 0+01145 0+01145 1+690E 22 1	-171+ 296- 59500- 0-00882- 0-00882- -301E-22_8	170. 296. 59500. 0.00553 0.00553	01. 294. 2884. 0.02132 0.02132	56. 296. 420. 0.01579 0.01579 1.645E 20	136+ 338+ 2884+ 0+02066 1+00395	133- 338- 2584- 0-02066 0-50000 1-294E 21	115- 336- 2664- 0-02079 0-02079 1-303E 21
(cn)-1				-			•	
428.00 428.20 428.49 428.60 428.30	41.594 41.727 41.861 41.997 42.145	35.815 35.918- 36.884 36.182 36.216	25.897 25.946 25.996 26.852 26.119	21.339 21.376 21.415 21.457 21.514	7.048 7.052 7.057 7.064 7.073	35.531 35.649 35.649 35.778 35.494	30.230 30.284 30.340 30.404 30.493	20.233- 20.261 20.291 20.323 20.367
429. # 0 429. 2 # 429. 4 0 429. 6 0 429. 8 0	42.298 42.444 42.582 42.717 42.853	36.339 36.454 36.555 36.653 36.752	26.192 26.255 26.389 26.368 26.414	21.576 21.625 21.665 21.785 21.743	7.002 7.090 7.097 7.103 7.107	35.017 36.120 36.202 36.278 36.356	30.594 30.673 30.730 38.761 30.633	28.421 20.464 28.495 28.524 28.552
430.00 430.20 430.60 430.60 430.80	42.992 43.135- 43.288 43.432 43.596	36.855 36.960 47.069 87.181 37.387	26.478 26.529 26.586 26.653 26.733	21.762 21.823 21.466 21.918 21.977	7.111 7.115 7.118 7.122 7.131	36.436 -36.524 36.519 36.731 36.473	30.848 38.949 31.817 31.897 31.286	20.593 20.618 20.692 20.697 28.732
431.00 431.20 431.40 431.60 431.89	43.779 43.971 44.163 44.343 44.507	37.463- 37.642 37.821- 37.979- 38.114	26,851 27.609 27.146 27.250 27.327	22.444 22.229 22.356 22.436 22.492	7.168 7.216 7.259 7.273 7.261	37.847 37.239 37.428 37.599 37.736	31.355 31.536 31.714 31.868 31.967	20.416 20.945 21.066 21.139 21.183
432.00 432.20 432.40 432.60 432.90	46.653 46.794 46.931 45.066 45.190	38.227 34.330 38.429 38.526 38.621	27.386 27.448 27.493 27.545 27.595	22.536 22.578 22.619 22.658 22.695	7.288 -7.296 7.303 7.310 -7.316	37.843 37.933 38.815 36.895 38.178	32.044 32.180 32.168 32.227 32.276	21.215 21.244 21.272 21.309 21.326
433.00 433.20 433.40 433.60 433.80	45.328 45.457 45.586 45.716 45.847	38.715 38.889 38.902 38.995 39.090	27.643 -27.650 27.738 27.706 27.836	22.730 22.766 22.884 22.442 22.440	7.326 7.324 7.329 7.334 7.337	38.243 38.315 38.399 38.468 38.554	32.326 32.375 -32.424 -32.476 32.532	21.350 21.375 21.400 21.427 21.455
434.00 434.20 434.60 434.66 434.68	45.988 45.118 46.266 46.427 46.609	39.187 39.287 39.396 39.529 39.668	27.887 27.942 28.807 28.181 28.226	22.918 22.958 23.068 23.069 25.211	7.348 7.344 7.352 7.374 7.417	35.650 38.762 38.762 39.478 39.478	32.597 32.674 32.775 32.914 -33.669	21.485 21.518 21.561 21.639 21.763
435.81 435.28 435.40 435.60 435.88	48.795 46.974 47.137 47.291 47.443	59.860 40.021 40.159 40.279 40.395	28.359- 28.471 28.553 28.617 28.631-	23.332 23.409 23.462 23.509 23.557	7.455 7.473 7.462 7.469 7.496	39,948	33.274 33.439 33.572 33.683 33.798	21.900 21.997 22.057 22.163 22.148
436.20 436.40 436.60 436.80	47.402 47.776 47.963 48.155 48.345	40.519 40.661- 40.828 41.012 41.191	26.757 28.868 29.999 29.153 29.267	23.615 23.784 23.839 23.989 24.108	7.504. 7.524 7.577. 7.688 Y.674	41,020 41,013	33.915 34.067 -34.249 34.448 34.625	22.205 22.294 22.439 22.590 22.716
437.00 437.20 437.40 437.60 437.80	43.528 43.677- 43.824 43.964 43.099	41.343 41.472 41.583: 41.684 41.783:	29.361 29.446 29.504 29.557 29.616	24.213 24.252 24.252 24.298 24.329	7.685 7.693 7.698 7.783 7.788		34.775 34.692 34.979 -35.651 35.118	22.767 22.635 22.671 22.902 22.938
439.80 439.20 436.40 436.60 436.80	49.235 49.372 49.508 49.643 49.772	41.884 41.986 42.087 42.184 52.276	29.666 29.723 29.777- 29.828 29.875	24.378 24.412 24.452 24.489 24.553	7.713 7.716 7.723 7.727 7.731	41:821 -41:902 -41:976 -42:647	35.1 84 35.247 35.385 35.356 35.483	22.967 23.071 23.232 23.868 23.863
439.80 439.20 439.40 439.60 439.80	49.901 58.431 58.164 58.296 59.426	42.366 42.458 42.553 42.648 42.739	29.922 29.972 38.623 50.673 80.121	24.716	7,734 7,738 7,744 7,750 -7,756	48.435	55.587 35.578 35.638 -35.683	23.139 23.175 23.208 23.232 23.256
440.20 440.20 440.60 440.60	58.554 58.683 58.812 58.943 51.878	42.829 42.916 43.089 43.182 43.199	30.167 30.214 30.261 30.318 30.361	24.751 24.766 24.422 24.866 24.298	7.761: 7.767 7.772 7.778 7.783	42 75 85 72 16 66 42 77 53 42 78 50	35.734 35.746 35.642 35.981 35.966	23.279 23.319 23.329 23.356
441.80 441.20 441.40 441.50 441.80	51.226 51.372 51.535 51.714 51.986	43.388 43.413 43.542 43.699 43.888	38.416 38.492 38.578 38.692 38.647	24.939 24.987 25.853 25.157 25.382	7.769 7.795 7.804 7.832 7.868	43.096 43.255 43.637 -43.631	36.134 36.254 36.449	23.418 23.468 23.551 23.682 23.851
442.00 442.20 442.48 442.60 442.00	52.102 52.300 52.496 52.696 52.067	44.874 44.271 44.462 44.636 44.789	31.029 31.215 31.301 31.500 31.605	25.479 25.458 25.489 25.988 25.975	8.046 8.102 9.120	46.029 46.228 46.618 46.597	36.983 37.176 27.358 37.498	24.022 24.161 24.244 24.303
443-80 443-28 443-40 443-60 443-80	53.039 53.209 53.347 53.574 53.768	44.929 45.867 45.216 45.389- 45.573	31.607 -31.773 -31.001 -32.021 -32.179	26.099 26.165 26.816 26.471 26.595	4.143 -4.158 4.205 4.268	45.133 45.133 45.329 45.527	37.779 37.941 38.125 36.328	24.426 24.518 24.652 24.815 24.953
444.88	53.960	45 (753:	32.321	2	-1004	1 7,1126		

^{45 (753:} *-The units of u are molecules/cm2, abbreviated here by (#/cm2).

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SECTION 5

ABSORPTION BY CO₂ BETWEEN 500 AND 850 cm⁻¹

SAMPLING

The temperatures and total pressures of the samples studied were varied over wide ranges representative of the earth's atmosphere. Samples varied in pressure from 1 atm to less than 0.03 atm and were maintained near one of three different temperatures: 310 K, 274 K, and 245 K. The highest temperature corresponds approximately to the maximum atmospheric temperature in the tropics. The lowest temperature, 245 K, approximately represents stratospheric temperatures. Ideally, somewhat lower temperatures should be employed to cover the full temperature range of the atmosphere; however, the experimental difficulties associated with operating at lower temperatures would greatly increase the time involved in obtaining the data and would also reduce the accuracy. As a compromise, the lower temperature of 245 K was chosen. An intermediate temperature near 274 K was also employed in order to provide additional data on the temperature dependence of the absorption.

All of the samples studied were contained in a multiple-pass absorption cell that has been described previously. The base length of the cell is I meter, and the optical path can be varied in increments of approximately 4 m up to a maximum of approximately 40 m. The number of passes of the monitoring beam can be adjusted externally without disturbing the sample in the cell. Electrical resistance wire coiled around the outside of the stainless steel body of the cell provides the heat when operating the cell above room temperature. The cell is well insulated so that only approximately 30 watts of power are required to maintain it at 310 K. When operating at this temperature, the gas in the cell is maintained uniform to less than ± 1 K. The temperature is controlled manually by adjusting the current through the heating wires.

The main body of the absorption cell is contained within a stainless steel tub that can be filled with liquid to submerge the cell. The intermediate temperature, 274 K, was maintained stable to + 0.5 K by filling the tub with ice-water. The lower temperature, approximately 245 K, was attained by submerging the cell in a mixture of commercial "anti-freeze" and water that was chilled by bubbling liquid nitrogen through it. A piece of copper tubing submerged in the bottom of the tub that contained the anti-freeze mixture carried the liquid nitro; en from a large commercial dewar. Ten holes located at different places along the tubing allowed the nitrogen to evaporate and bubble from the tubing through the liquid. The movement of the bubbles mixed the liquid enough to maintain the temperature throughout the length of the absorption cell constant to approximately \pm 1 K. The cell temperature was controlled by adjusting the rate of flow of the liquid mitrogen. After the cell temperature had been reasonably well stabilized, the temperature could be maintained constant to within ± 1 K for several hours. The low-temperature samples varied from approximately 243 to approximately 249 K. It was not important that all of the samples be at exactly the same temperature as long as

the temperature was measured accurately. Therefore, if the cell temperature was stabilized within this range, no effort was made to readjust the temperature. The stability of the optical system, and thus the accuracy of the data, are strongly dependent on temperature gradients and temperature changes in the cell.

A few of the data were obtained for samples of pure CO2; most of the data represent samples of CO2 mixed with dry air. The dry air consists of 79% N2 and 21% O2 to match the atmosphere. The mixtures of CO2 plus dry air were obtained pre-mixed from a commercial gas supplier in cylinders at total pressures of approximately 150 atm. Table 8 lists the concentrations, in mole percent, of the different mixtures studied. The values of CO2 concentration listed in the left-hand column are those determined spectroscopically by us in the laboratory before any spectral data were obtained; these values are the ones used in calculating the absorber thickness of the samples. The concentrations listed in the second column from the left are those provided by the gas supplier. Five of the eight measured concentrations agreed with the values provided by the gas supplier to within our measurement accuracy.

The concentration of each mixture was checked carefully by comparing its infrared absorption to that of a laboratory-mixed sample with very nearly the same concentration of CO2. Samples used in these concentration measurements ordinarily varied in pressure from approximately 0.3 atm to 1 atm because pressures in this range can be measured quite accurately. The sample cell was at room temperature and was adjusted to either 4 or 8 passes in order to attain good stability. The spectrometer slits were adjusted wide to smooth out most of the structure in the spectrum over the short spectral interval used for the concentration measurements. The spectral interval was chosen so that the absorptance was nearly constant over the interval and was between approximately 0.4 and 0.7. With the absorptance in this range, the smallest fractional difference in the CO2 concentration could be detected. Each measurement was repeated several times. Two separate batches of laboratory mixtures were made for each concentration, and the absorption by a given pressure of gas from each batch was compared. If the agreement between the measurements for a given concentration was not excellent, a new batch was made and the measurements were repeated.

The laboratory mixtures were made by introducing carefully measured amounts of CO₂ and dry air into a glass-lined mix-tank. The mix-tank is supplied with a small mixing blade that is driven from outside the tank by a drill motor. The shaft on which the mixing blade is mounted extends through a rotating seal that employs lubricated "O-rings". Partial pressures of the CO₂ and the dry air introduced into the mix tank could be measured with an accuracy of approximately 0.1 to 0.2%. The total pressure of the mixture was typically 10 atm. The estimated uncertainty in the values assigned to the concentrations for each of the laboratory mixtures varies from approximately 0.2% of the concentration for the higher concentrations to 0.5% for the lower concentrations. The laboratory-mixed samples were employed only to check the concentrations of the commercial mixtures, which were employed for all of the samples for which spectral data are presented.

No evidence of systematic error due to selective adsorption of CO2 on the walls of the sample cell could be observed. The possibility of this phenomenon occurring was checked carefully for the most dilute (0.125% CO2) mixture. Errors due to adsorption would probably be largest in the dilute samples. ing the tests for adsorption, the infrared absorption at a fixed wavelength was measured, starting immediately after a sample had been introduced into the sample cell. Approximately one minute was required for the apparent absorption to stabilize because of the changing temperature of the gas as it expanded into a reviously evacuated cell. After this short period of stabilization, the absorption by a sample remained constant for several days and was the same as the absorption by a sample of the same concentration that was flushed continuously through the cell. We concluded that no significant errors were being introduced by the adsorption and desorption of CO_2 from the cell walls. Some evidence of adsorption and desorption could be observed under extreme conditions that did not apply to our sampling procedures. For example, if the cell were filled with I atm of pure CO2, then evacuated quickly to less than I torr of pressure, a slight increase in the infrared absorption could be observed for a few minutes after the valve to the pump was closed. This increase in absorption was apparently due to a small amount of CO2 desorbing from the walls of the cell. However, we made certain that the cell was out-gassed before introducing a dilute mixture into the cell for investigation.

Three different gauges measured the sample pressures. A mercury manometer served for pressures between 0.1 and 1 atm, an oil manometer for pressures between approximately 0.003 and 0.1 atm, and a McLeod gauge for lower pressures. The parameters of the samples studied are summarized in Table 8. As explained above, the concentrations of the mixtures of CO2 plus dry air used to determine sample absorber thicknesses are given in the left-hand column. Only a few data were obtained for samples of 100% CO2; these are summarized in the upper portion of Table 8. The three right-hand columns of the table correspond to the three sample temperatures employed. For the 100% CO2 samples, the pressures listed under a given temperature correspond to the samples for which spectral data were scanned. Not all of the samples of CO2 plus dry air are represented in the table. A series of samples at different equivalent pressures were studied for each combination of path length and concentration. The maximum equivalent pressure for each series was 1.00 atm; each succeeding equivalent pressure was reduced by approximately a factor of two, giving pressures of 0.500, 0.250, 0.125 atm, etc. Only the lowest pressure is listed in Table 8 for the mixtures. In some cases, particularly for the lower pressures, the equivalent pressures were not adjusted to exactly an integral power of 0.5 atm; the measured pressures were used to calculate absorber thicknesses. The exact parameters for each sample are listed below in tables that include detailed results.

SPECTROSCOPIC PROCEDURES

The procedures employed in scanning the spectral data are essentially the same as those used to obtain the data presented in Sections 2 and 4. All of the optical path external to the sample cell passed either through a vacuum or through non-absorbing N₂ to eliminate absorption by CO₂ or any other atmospheric gas. The grating employed for the CO₂ data contains 40 grooves/mm and is blazed for maximum efficiency at 22 μ m. All orders of wavelengths except for the first order were eliminated by a KBr prism.

TABLE 8. SUMMARY OF SAMPLES

				Minimum				
%	%	Path	E	quivalent Pre	ssure			
co ₂	CO ₂	Length		(atm)				
(Measured)	(Gas Supplier)	(cm ⁻¹)		Temperatur	·e			
(ileasurea)	dappizery	(0)	310K	274K	245K			
	100*	3291	1.00*	1.00*	1.00*			
	100	3291	0.500*	0.500*				
	100	3291	0.250*	0.250*				
	100	3291	0.125*					
	100	3291	0.00198*					
	100	3291	0.00393*					
**************************************					-			
15.3	15.3	3291	0.00198	0.00195	0.00193			
8.09	8.09	3291	0.00197		-			
3.85	3.85	3291	0.00194	0.00192	0.00386			
3.85	3.85	1648	0.00386					
1.91	1.91	1648	0.00781	0.00781	0.00781			
0.977	0.977	1648	0.00779					
0.503	0.511	1648	0.0157	0.0157	0.0157			
0.250	Ò.260	1648	0 . 0 1 5 5	-				
0.125	0.128	1648	0.0313	0.0313	0.0313			
0.125	0.128	826	0.0619	0.0625	0.0625			

^{*} The pure (100%) CO₂ samples are from a cylinder of commercial grade CO₂ with purity reportedly greater than 99.5%. The equivalent pressures listed for pure CO₂ represent all of the pure CO₂ samples studied. A series of samples at different equivalent pressures were studied for each combination of path length and concentration of the CO₂+ dry air mixtures. The equivalent pressures for each series were 1.00 atm, 0.500 atm, 0.250 atm, etc. down to the equivalent pressure tabulated.

A background curve that corresponded to 100% transmittance was scanned with the sample cell evacuated, either immediately before or after each sample spectrum was scanned. In order to check for possible sampling errors or changes in the signal level corresponding to 100% transmittance during a scan, portions of each spectrum were re-run and the results were compared with the spectrum that was to be reduced further. Separate samples having the same parameters were employed in the comparisons as further checks for possible sampling errors. Each sample spectrum and its corresponding background spectrum were digitized with the data related directly to detector signal punched on computer cards. A computer then calculated values of transmittance, integrated absorptance, etc.

The spectral slitwidth was adjusted wide enough to smooth out most of the structure due to individual vibration-rotation lines in the P- and R-branches of the bands. The Q-branches appear as single absorption features in the spectra. Smoothing the spectra in this manner simplifies the reduction and analysis of the data while maintaining adequate resolution for quantitative comparison with calculated spectra. The physical widths of both the entrance and exit slits of the grating monochromator were fixed at 1.7 mm. This resulted in the spectral slitwidth changing with wavenumber as given in Table 9. The values tabulated represent the full width at half-maximum of a triangular slit function. As can be seen in the transmittance curves shown below in this section, a small amount of structure remains in some of the P- and R-branches because of the individual lines. Slightly wider slits would have smoothed out this remaining structure as was originally intended. However, further widening the slits beyond the 1.7 mm used would have produced an irregular and unknown slit function for two reasons: The image of the Nernst glower source formed at the entrance slit was not sufficiently wide to illuminate a wider slit uniformly. In addition, the image of a wider exit slit formed on the detector would have overfilled the sensitive element of the detector. It is apparent that the outer portions of wider slits would not contribute properly to the detector signal, thus producing an irregular slit function. Interchanging or readjusting the optical components to overcome this problem so that wider slits could be used was not believed to be justified because of the small amount of undesired residual structure in the spectra.

A few checks were made on the uniformity of the sensitivity of the instrument to different narrow portions of the 1.7 mm wide slits that were used. The non-uniformities that were observed could lead to effective spectral slitwidths that differ by no more than 5 to 10% from the values listed in Table 9. Non-symmetry of the sensitivity about the center of the slit can also lead to slight shifts in the effective center of the spectral band passed by the slits. This phenomenon can lead to apparent shifts in the calibration that relates wavenumber to grating position as the slitwidth is changed. Errors in wavenumber calibration due to such non-uniformity in sensitivity could not be larger than 10% of the spectral slit width.

Table 10 lists the absorption lines used to provide wavenumber calibration. Transmission spectra of the calibration gases were scanned with the spectral slitwidths adjusted to about one-fourth of the values listed in Table 9. The calibration lines were well resolved with this improved resolution. The line positions were determined in terms of fiducial marks that were related directly

TABLE 9. RESOLUTION SCHEDULE

ν	Spectral Slitwidth
-(cm ⁻¹)	(cm ⁻¹)
500	1.2
550	1.5
600	1.9
650	2.3
700	2.7
/50	3.2
800	3.6
850	4.2

TABLE 10. CALIBRATION DATA

ν _ō		·vo	
(cm ⁻¹)	-Ģás	(cm ⁻¹)	Gas
481.5	extrapolation	633.87	co ₂
494.19	́н ₂ 0	645.86	co ₂
506.93		661.16	co ₂
519.60	́Н ₂ O -ĭН ₂ O	674.44	co ₂
525.98	:Ḥ ₂ 0	687.16	·co ₂
536.26	.H20	700 . 06-	-co ₂
547.83	т <mark>2</mark> 0	725.4 7	co_2
554.64	H ₂ 0	743.83	co ₂
567.23	H ₂ 0	760,27	co ₂
576.14	-Ĥ ₂ 0	775.81	·co ₂
584.74	H ₂ 0	788.32	co ₂
594.96	:Н ₂ 0	806.26	co ₂
604.46	H ₂ 0	826.51	co ₂
620.59	H ₂ 0	-860-0-	extrapolation

to grating position. It was assumed that the relationship between wavenumber and grating position remained fixed when the slits were widened to scan the spectral data. The errors introduced by making this assumption are essentially those caused by the non-uniformities in slit illumination discussed in the previous paragraph. The CO₂ line positions are well-known throughout most of the spectral region and were used from approximately 630 cm⁻¹ to the high-wavenumber side of the band. All of the wavenumbers listed in Table 10 from 633.87 to 826.51 cm⁻¹ correspond to the centers of CO2 lines that are not "blended" with weaker adjacent lines enough to shift the apparent line centers significantly. The CO2 line positions listed are from a report by Drayson. 13 No easily identifiable absorption line was available as a calibration standard near 850 cm⁻¹, the high wavenumber limit of the region of interest. Therefore, the position of a "false" line at $860.0~\mathrm{cm}^{-1}$ on each spectrum was determined by extrapolation and used as a standard. Accurate calibration is not critical between 826 and 850 cm⁻¹ because of the small amount of absorption and the lack of spectral structure in this region.

Absorption lines of H₂O were employed for the low-wavenumber side of the region. The H₂O kines used are reasonably well isolated from other lines so that the center positions can be located accurately and the points of maximum absorption are nearly independent of the slitwidth. Many of the CŌ2 lines in the 490-625 cm⁻¹ region are blended, making it difficult to determine their center positions accurately. All of the H₂O line positions from 494.19 to 620.59 cm⁻¹ are from unpublished data provided by W. S. Benedict and R. F. Calfee. Have the values listed for these lines agree within a few hundredths of a cm⁻¹ with the corresponding values in the AFGL listing of line parameters (Ref. 1). The "false" line at 481.5 cm was located by extrapolation in the same manner as that used for the 860.0 cm⁻¹ line. A spectrum of N₂O was scanned, and the known positions of the lines were used to confirm the positions of the H₂O lines between 590 and 634 cm⁻¹. The 6.3 μm H₂O band was scanned in 2nd order and its line positions used to confirm the calibration from 670 to 730 cm⁻¹.

Before each recorded spectrum was digitized, the positions of the calibration lines were marked on the recording. During the digitizing process, the positions of these calibration lines were also digitized in terms of their physical position on the recording. Wavenumber positions between the calibration lines were computed by interpolating on a linear wavenumber scale. The maximum error introduced by the assumption of a linear wavenumber scale was

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¹³S. R. Drayson, "A Listing of Wavenumbers and Intensities of Carbon Dioxide Absorption Lines Between 12 and 20 μm." Technical Report 036350-4-T, National Aeronautics and Space Administration, Contract No. NSR 23-005-376, May 1973.

W. S. Benedict, Inst. for Molecular Physics, College Park Maryland, 90742; R. Calfee, Wave Propogation Labs., Environmental Research Labs. National Oceanic Atmospheric Administration, Boulder Colorad. 80302, (Private Communication).

approximately 0.1 cm⁻¹. The estimated total error in wavenumber calibration is less than 0.2 cm⁻¹ for most of the spectrum, but it may be as large as 0.4 cm⁻¹ in a few places.

RESULTS

The results of the CO2 transmission measurements are presented in detail in the form of tables of integrated absorptance, Adv, and in spectral plots of transmittance. Tables 12 through 27 contain extensive lists of the cumulative value of the integral Adv. Table 11 summarizes the samples represented and the wavenumber interval covered by Tables 12 - 27. The table is divided into three sections, one section for each temperature. The first letter of each sample number identifies the temperature as follows: H, 310K; Z, 274K; L, 245K. The second letter identifies a group of samples for which the corresponding spectra were processed together. Several groups may cover the same spectral region, and the data appear in a single table. As examples, HBO1, 2 refers to two samples: HBO1 and HBO2; HCO1-3 refers to samples HCO1-3 refers to samples HCO1, HCO2 and HCO3. The two right-hand columns of each section of Table 11 lists the number of the table that the integral values appear and the figure number that the spectra appear for each sample.

Each column in Tables 12 - 27 corresponds to a given sample with the sample parameters listed at the top of the column. The molar concentrations of $\rm CO_2$ in the mixtures with dry air are listed along with temperature, path length, total pressure, equivalent pressure $\rm P_e$ (see Equation (8)), and absorber thickness. The pressures were originally measured in torr, and the values were submitted to the computer with the appropriate number of significant figures. Values of the pressures were computed in atm and listed in the table without rounding them off to the corresponding number of significant figures. For the same reason, many values of absorber are also listed to more than the significant number of figures.

The lower limit of integration, v', is lower for large samples that absorb a measurable amount far into the wings of the band system that it is for small samples. The tabulated value for a given wavenumber v represents the value of the integral from v' up to v. Successive values of v differ by 2 cm⁻¹; the maximum value of v listed depends on the amount of absorption by the sample. Several samples absorb a small, but measurable amount beyond the spectral limits included in Tables 12 - 27. The data for these samples have been omitted in the wings of the band system because data for larger samples provide more accurate checks on line parameters. When the absorptance is small, very slight errors in placing the 100% transmittance curve can result in large relative errors in the apparent line intensities.

The integrated absorptance between any two wavenumbers listed in Tables 12 - 27 is equal to the difference between the tabulated values of the integral. Some deviation from the true integrated absorptance that would be observed with infinite resolving power occurs because of the finite slitwidth employed in scanning the spectra. Enough significant figures are carried in the integral values so that the difference between two successive values retains all of the significant figures justified by the accuracy of the original data.

Computer plots of transmittance for the samples are shown in Figures 10-24. The spectral resolution is the same as that of the original spectra (Table 9) that were scanned and recorded by a strip-chart recorder. Only three of the parameters for each sample are given in the figures. The listings appear in the same order, top to bottom, as the spectral curves. Values of absorber thickness v are expressed in exponential form. For example, 1.528E 18 indicates 1.528 x 10¹⁸ molecules/cm². All of the samples represented in Figures 10 - 16 were near 310K; Figures 17 - 20, near 274K; and Figures 21 - 24, near 245K.

Values of P_e and P are related by Equation (8) with B = 1.30; these two values of pressure approach each other for very dilute mixtures of CO_2 in dry air. In a few spectral regions within the band system, a significant portion of the absorption may be due to the extreme wings of distant Fines. In these cases the value of B = 1.30 on which P_e is based may not be appropriate (see Reference 3). The path lengths and CO_2 concentrations are not given in Figures 16 - 24, but they can be found in the headings of Tables 12 - 27.

TABLE 11. SUPPMARY OF TABLES AND FIGURES

	l	Fig.	.														
		1		21 72	21 2	21	22	3 8	3 5	22	21	22	22	70	24		
		Table	<u>i</u> i	# 7				ď	Ç		26			27	27		
	77.8	To - 00	000 000	007-007			590-750			610-735		656-680		500-560	780-850		
		Sample	1.401	LB02	LC01,3 LD02,4	LE01,3,5	LF02,4,6 LG01,3,5,7	LH02.4.6.8	LI01,3,5,7,9	1,301,2,4,6,8,10	LK01,2,4,6,8	LEO1,2,4,6 LMO1,2,4	LN01,2	1041	1001	_	
IGURES		Fig.	17	17	17	17	61	19	19	18	17	17	18	20	20		
S AND F		Table No.	62					20			21			22	23		
SUMMARY OF TABLES AND FIGURES	274 K	vo - vL (cm-1)	560-780				590-750	590-750		610-735	610-735	656-680		200-560	780~850		
TABLE 11. SUMMA		Sample No.	2A01	ZB02 ZC01.3	ZD02,4	ZE01,3,5 ZF02,4,6	2601,3,5,7	ZH02,4,6,8	2101,3,5,7,9	7701,2,4,6,8,10	ZK01,2,4,6,8 ZL01,2,4,6,8	ZMO1,2,4	Z, 10nz	ZP01-6	9-1002		
		F1g. No.	10	0 02	01;	2 11	11	ដ	12,13			14,15		01	91	16	
		Table No.	12				13		14		15	91			17	18	
	i	% - %t (cm - ½	560-780				560-780		590-750		610-735	610-735	656-680	020-020	200-560	780-850	
		Sample No.	11,01,2	nnot, 2	HC01-3 HD01-4	11501-5	11F01-6	HG01-7	RH01-8	H101-9	11J01-10 IIK01-9	HL01-8	HNOL-5	100 C - 700 C - 700 C	HP01-5,7,9	11Q01-2,3,4,6,8	

	HE05 310, 3291, 0,15300 0,059737 0,062479 7,125E 20		0.00 0.00 0.052 0.099	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.667 0.369 1.627 1.221	1.657 1.975 2.149 2.520 5.260	5.665 7.936 ** 3.55 ** 7.71 5.149	5.595 6.019 6.176 7.159 8.561	9.551 10.631 10.573 11.273	12 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	19.460 20.919 22.196 73.913	27.36° 29.206 31.016 32.913
	HE04 310. 3291. 0.00093 0.121711 0.12464		0.00 1.946 0.067 0.104	5 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	0.701 1.913 1.159 1.564	2.922 2.536 2.541 3.023 4.474	**356 **356 5*205 5*690 6*221	6.765 7.306 7.972 3.691 13.221	11.262	15.635 16.967 19.923 21.529	23.152 24.457 25.543 2*.281 30.074	32.316 33.952 35.991 37.903 39.721
	HE03 310. 3291. 0.03850 0.247368 0.250226 7.425E 20		\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$	3.36 3.36 3.56 3.76 3.72 3.72	0.910 1.160 1.450 1.736 7.064	2.426 2.529 3.276 3.840	5.444 5.991 6.502 7.221 7.909	9.512 9.317 12.047 11.036	13.653 14.631 15.564 16.693 17.992	19.656 21.051 22.752 24.503 26.309	29.167 30.021 31.499 33.882	37.721 39.710 41.655 43.662
	HEOZ 310. 1648. 0.01850 1.194074 0.492786		000000000000000000000000000000000000000	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.570 1.145 1.465 1.466	2.6811 3.6811 5.6811 5.295	6.179 6.385 7.646 8.446 8.433	13.191 11.069 11.962 13.060	16.133 17.125 19.266 19.626 21.177	22.570 24.671 26.536 28.43 36.36	32.322 34.263 36.251 39.231	62.225 66.222 68.222 68.222
	HE01 310. 16.0 0.01.910 0.994737 1.00.947		0.020	**************************************	0.941 1.246 1.603 2.603	3.600 4.610 6.305 5.135 6.375	7.379 8.299 9.275 10.305	12.43 13.574 16.674 151961	19.296 20.443 71.915 23.418 25.199	27.068 29.946 30.941 32.913 34.899	86.898 68.898 68.898 88.898 88.898	56.43 57.63
	9914 310- 3491- 0-15406 0-119737 0-125241		0.055 0.134 0.190 0.190	00.39	1.297	7 100 E	6.626 7.227 7.227 7.226 7.236 8.594	10.955 11.783 12.910 12.910	15.365 16.705 17.495 19.975	21.735 23.343 25.12. 26.913 29.751	20.553 36.553 36.510 36.510 36.510	100 100 100 100 100 100 100 100 100 100
	H)013 3100 32910 0.244079 0.250003 1.539E 21		0.000 0.100 0.171 0.271	0.50 0.50 0.50 0.90 0.90 0.90 0.90 0.90	1.441 2.269 2.769 3.209	4.74 5.0037 5.0027 7.0062	7.967 9.720 9.601 10.518	12.506 13.519 14.561 17.731	19.034.20.134.21.367.22.620	2002 2002 2002 2002 2002 2002 2002 200	35.058 37.029 39.911 61.506 63.796	45.796 47.796 49.796 51.796 51.796
Αď	HOG2 310- 3291- 0-01850 0-493421 0-499220		0.105	10.954 10	1.6576 2.654 3.102 3.701	5.9994 6.9994 7.9994 7.999	9. 4.66 110. 4.69 12. 6.69 13. 90.4	15.037 16.273 17.529 19.012	22.494 23.767 25.730 26.931 26.941	30.646 32.604 34.579 36.564 38.564	40.567 42.567 44.567 46.567	50.567 52.567 54.567 56.567
12 J.W	HUDI 310. 1648. 0.03850 0.986816 1.000237		00000 00000 00000 00000 00000	1.023	12.22.4	1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	18-924 12-172 13-690 14-867 16-310	17.771 19.242 20.729 22.367 24.299	26.056 27.549 29.222 31.063	36.936 36.936 36.936 50.936	44.976 46.976 48.976 50.976	54.976 56.976 58.976 63.976
TABLE I	HCO: 310- 3241- 0-15300 0-23KH15- 0-23KH15- 0-249T77		60.00 60.00 60.00 60.00	0 125 11.245 11.245 2.654 2.65	2.40 4.00 4.00 6.00 6.00 6.00 6.00 6.00 6	5.448 7.602 7.602 9.760	11.476 12.575 13.749 14.997	17.678 19.039 20.536 22.052 23.987	25.636 26.356 25.436 30.153 32.058	33.933 37.947 37.947 39.945 41.945	643.0458 644.0458 640.0458 640.0458	53.945 55.945 57.945 59.945 61.945
1	MCO2 310- 3291- 0-06090 0-488158 0-5007-5		0.1109	0.024 1.105 1.453 1.929 2.329	2.560 3.609 4.394 5.191	7.039 8.032 9.232 10.576 12.269	13.676 15.026 16.462 17.968	21-11-6 22-763 22-4-607 22-6-202 22-6-202 23-6-202 20-2000 23-6-2000 23-6-2000 23-6-2000 23-6-2000 23-6-2000 23-	29.976 31.559 33.251 35.171	45.1125 45.1125 45.1125 45.1125 45.1125	49.125 53.125 53.125 55.125 57.125	59.125 61.125 63.125 65.125 67.125
	HC01 310, 3291, 0,03530 0,998138 0,99571		00.009	11.555	6444 6444 6444 6444 6444 6444 6444 644	7.995 9.247 10.615 12.144 13.956	15.603 17.210 18.879 28.608 22.370	24-159 25-963 27-737 29-697 31-677	35.337 35.337 37.269 39.232	45.227 47.227 49.227	53.227 55.227 57.227 59.227 61.227	65.227 65.227 67.227 69.227
	HB02 310. 3291. 0.15300 0.477632 0.499555 5.697E 21		4.11.72	1.4447 2.456 2.956 3.651	5.547G 5.547G 7.6666 8.566	10.120 11.666 12.926 14.569	15.197 19.931 21.620 73.409	25.000 25.0000 25.000 25.000 25.000 25.000 25.000 25.000 25.000 25.000 25.0000 25.000 25.000 25.000 25.000 25.000 25.000 25.000 25.000 25.0000 25.000 25.000 25.000 25.000 25.000 25.000 25.000 25.000 25.0000 25.000 25.000 25.000 25.000 25.000 25.000 25.000 25.000 25.0000 25.0000 25.000 25.000 25.000 25.000 25.000 25.000 25.000 25.000 25.0000 25.000 25.000 25.000 25.000 25.000 25.000 25.000 25.000 25.0000 25.000 25.000 25.000 25.000 25.000 25.000 25.000 25.000 25.0000 25.000	36.772 35.698 40.568 42.476	66.6443 50.6443 50.6443 50.6443	56. 56. 57. 57. 57. 57. 57. 57. 57. 57. 57. 57	66.473 68.473 78.473 72.473
	HB01 310. 3291. 0.08090 0.976316 1.000011 6.158E 21		######################################	1.55 2.4115 7.4115 7.429 8.428	5.241 6.4464 7.4664 10.654	12.030 113.669 17.740 19.194	21.089 22.967 24.976 26.987 26.987	30.719 32.684 36.684 36.655	60.666 60.666 60.576 66.576 68.576	50.576 52.576 54.576 56.576 58.576	60.576 52.576 54.576 66.576 65.576	70.576 72.576 74.576 76.576 76.576
	HA01 310, 3291, 0,15300 0,95263 0,99110 1,139E 22		2000 2000 2000 2000 2000 2000 2000 200	8 4 4 8 4 8 4 8 4 8 4 8 4 8 4 8 8 8 8 8	7.899 9.899 11.069 12.679 14.618	16.226 18.030 28.003 21.969 21.969	25.965 27.953 29.953 31.953 33.953	2000 2000 2000 2000 2000 2000 2000 200	65.953 67.953 69.953 51.955 53.955	55.555 57.455 59.455 61.4955	65.953 67.953 69.953 71.953	75.954 77.454 77.454 74.454 81.954 81.954
	HF02 310. 3291. 1.00.00 0.00.3026 0.00.3434		7 W N 0 0 0 0 0 0 0 0 0 3	00000 00000 00000 00000 00000 00000 0000	0.161 0.267 0.255 0.292 0.333	0.579 6.479 0.479 0.479	0.949 0.949 0.949 0.949 0.949	1.153	201.25	2.000 2.000 3.110 3.110 6.00 6.00	3.979 6.175 6.696 5.293	6.027 6.406 7.059 7.547
	310. 310. 3291. 1.0030 0.00126 0.001984		*****		0 - 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 100 0 1179 0 1158 0 1158 0 266	0.299 6.324 0.354 0.354 0.491	**************************************	1.696 1.152 1.216 1.233	H.5652 H.56761 H.56761 H.56761	2.037 2.037 2.035 2.596 3.035 3.035 3.035	2444 2444 2444 2444 2444 2444 2444 244
	Sea. No. Temp (X) Path (cm) Conc. F (atm) P. (atm) L (b/cm)	(ca ^{,1})	560.00 560.00 560.00 565.00 565.00	572.02 572.03 576.03 576.03 579.00	596.00 546.00 546.00 596.00 599.00	597.02 597.00 597.00 595.00 595.00	625.00 625.00 505.00 505.00 605.00 605.00	614.56 512.06 614.00 615.00	624.00 624.00 624.00 626.00	630.00 632.00 636.00 634.00	6.6.00 6.6.00 6.6.000 6.6.000	6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6

86.375 83.075 83.075 64.0675 64.0675	.5.71 .7.663 .9.517 51.337	56.36 56.753 53.653 62.055	55.736 57.653 56.553 70.539	71.369 72.641 73.965 75.091	70.967 77.731 78.515 79.159	52.561 52.561 52.996 53.371	4 6 4 6 4 6 4 6 4 6 4 6 4 6 4 6 6 6 6 6	36.371 97.027 37.629 47.917	33.63 33.63 33.93 33.36 39.36 39.36 36 36	40.697 40.697 40.474 40.054	96,11	36. 46	
14 16 16 16 16 16 16 16 16 16 16 16 16 16	51.399 53.395 55.336 57.276 59.231	61.1%5 63.37% 66.995 66.899	74.666 72.535 74.320 76.042	79.269 30.326 32.326 33.695 9595	85.991 87.010 87.916 85.710	490 93.065 93.065 93.065 93.065	95.565	97.12? 97.95. 93.502 93.943	94.549	100.976 101.032 101.170 181.291	101-55. 101-55. 101-609 101-609	101.74	
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52.2.2 56.2.2.2 59.2.2 59.2.2	62.22 64.222 66.222 69.227 73.222	72.22 74.222 76.727 79.222	92.222 90.222 90.221 93.205	92.113 96.0113 96.003 97.659	131.326 102.925 10372 105.657	108.496 110.295 111.295 112.943	113.673 114.533 115.756 126.249	113-006 119-13- 126-150 120-798 121-565	121-906. 122-396 122-367 123-254 123-636	124.169 124.169 124.361 124.515	124. 124. 124. 124. 124. 125. 125.	125.073	
55 55 55 55 55 55 55 55 55 55 55 55 55	66.693 70.693 72.693 74.993	76.693	24 7 7 7 9 2 4 7 7 9 2 4 5 6 9 2 4 5 6 9 2 4 5 6 9 2 4 5 6 9	26.52 26.52	165-662 108-472 110-154 111-657	116.976 116.703 117.592 118.513	120.936 121.936 128.014 126.199	126.317 127.639 129.936 179.696 130.443	131.754 137.754 157.303 137.792 153.213	153.548 155.601 154.072 154.160	136.516	134.754	
50.213 52.237 54.197 56.197	62-197 62-197 64-197 66-197 85-197	72.197 72.197 76.197 76.196	81.159 82.159 85.0375 85.095	63.691 91.505 93.301 94.357	97.920 99.235 157.516 161.637	105-35- 105-352 105-374 107-615	109-059 109-443 111-255 111-255	112.94- 115.97- 115.337 115.350	116. 1176.754 1176.754 1177.559	115.167 115.602 116.579 119.036	119.00 119.01 119.01 119.73 119.13 119.13	119.990	
55.736 57.736 59.736 51.736	65.796 67.736 69.796 71.796	75.796 77.75 79.756 81.736	95.746 47.746 49.745 91.745	95.716 97.672 99.615 101.676	106.977 105.514 109.490 119.774	112-511 114-277 115-376 116-246 117-145	119.036 119.036 119.331 120.415	25.931 125.132 125.132 125.132	127, 363 127, 363 129, 146 129, 125	129.790 129.790 130.22 130.240	130.571 130.707 1370.707 130.596	131.038	
60.567 62.567 64.567 65.567	70.567 74.567 74.567 76.567	30.567 31.567 34.567 34.567	90.567 92.567 94.567 98.567 94.567	100.567 102.567 104.567 105.539	113.357 113.926 113.926 115.562 117.154	113.995	125.531 126.716 127.904 129.091	131.510 137.995 134.751 135.130	137-159 137-159 139-124 139-124 139-329	339.726 364.156 164.667 160.726 160,957	161.245 141.245 141.643 161.543	141.690	
66.976 86.976 55.976 73.976 72.976	76.976 76.976 75.976 50.976 52.976	96.976 95.976 93.976 93.975	9+.976 96.978 95.976 101.976	104.976 106.976 105.976 110.976	114.965 116.927 113.542 123.616 122.338	124.293 126.195 127.633 129.010	131.7.48 133.17.48 134.625 136.670 137.516	139.647 142.649 142.097 143.226	145.243 146.944 146.944 146.944 147.9	164.965 149.273 169.510 164.936 150.124	150 . 325 150 . 433 150 . 673 150 . 7 27 150 . 817	150.097	
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69.128 73.128 75.128 75.128	79.125 631.125 95.125 97.125	94.125 93.125 93.125 95.125	99-125	109-129 1111-129 1113-129 115-129	119-122 121-097 123-015 124-895 126-66	125.636 131.567 132.139 133.643	139.160 139.160 139.160 141.740 147.741	146.171 147.6171 147.674 143.464	151,079 152,101 153,162 153,939 154,755	155.465 156.004 156.476 156.86 157.251	157.575 157.575 157.365 153.106 153.259	158.587	
75.227 75.227 77.227 79.227 31.227	93.227 15.227 81.227 19.227	93.227 95.227 99.227 101.227	165-227 165-227 107-227 119-227	113.227 115.227 117.227 119.227	125,227 125,227 127,713 129,175 131,119	135.097 135.071 136.390 139.569	141.539 143.742 145.507 147.279 149.054	\$25.358 \$2.358 \$5.358 \$5.568 \$5.568 \$5.58 \$5.58	159.639 159.373 161.025 162.094 153.031	153.23 154.523 165.073 165.548 165.943	166,292 166,592 156,529 167,415	167.299	
76. 79. 70. 70. 70. 70. 70. 70. 70. 70. 70. 70	######################################	96.473 99.473 100.473 100.473 100.473	106.173	1156.473 120.473 120.473 122.473 124.473	126.473	1 15. 334 1 35. 334 1 60. 245 1 62. 626 1 62. 626 1 63. 63. 63. 63. 63. 63. 63. 63. 63. 63.	165.611 147.625 149.252 151.031 152.976	156.745 156.745 159.573 160.069 161.546	154.976 154.86 165.626 166.845 169.042	169.022 169.932 170.496 171.175	172.246 172.246 173.230 173.543 173.926	174.070	
90.576 97.576 94.575 94.576 94.576	90.576 97.576 94.576 96.576	100.576 152.576 16.576 106.576	112.576 112.576 116.575 116.576	170.576 172.576 124.576 126.576 125.576	130.576 132.576 136.576 136.576	142.576 142.575 114.592 146.471	150.335 152.232 154.236 156.154 155.154	156.124 162.134 163.999 165.793 1e7.546	169-167 170-754 172-257 173-679 175-042	177.120 177.944 177.944 177.944	179,940 180,547 180,987 191,485	161.905	by (#/cm²)
95.953 97.953 99.953 91.953	95.953 97.953 93.953 101.953	167-953 167-953 163-953 111-953 111-953	115.953 117.953 114.953 121.953	127.953 127.953 129.953 131.953	137.953 137.953 139.953 161.953	165.953 167.953 167.953 151.953 151.953	154.953 157.953 159.953 161.953	165.953 167.953 169.945 171.901	175.718 177.562 179.355 191.095	136.295 185.592 156.741 187.793	153,457 191.651 192.071 192.53	193.248	abbreviated here
9.00 9.00 9.00 10.00 10.00 10.00	13.227	15.620 16.052 16.052 16.952	17.596	15.901 19.214 19.669 19.665	19.952 20.053 20.059 20.45 21.315 20.515	21.173	21.502 21.555 21.657 21.659	21.947 22.401 22.123 22.173 22.173	22.249	22.54.7	22.653 27.653 27.653 27.653 27.653	22.701	/c∎²,
51.158	7.000.	40000 40000 40000 40000 40000	100:00 100 1	12.716 13.914 10.959 11.065	11.227	11.633	12-117 12-153 12-2-1 12-2-1	12.3.31	12.576 12.404 12.426 12.545 12.545	12.537	12.734 12.734 12.734 12.734	12.734	of u are molecules
9667.45 9667.45 9667.46 97.96	677.0° 576.0° 676.0° 678.0° 673.0°	6 9 9 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	691.91 697.6. 594.03 695.30	7777	712.03 714.03 714.03 714.03	755.50	755.00 757.00 756.00 755.00 754.00	776 U 2 700 C 0 301 2 F 311 1 1 400 C 0	75000 75000 75000 75000 75000 75000 75000	765.65 765.65 765.64 765.05	772.00 772.00 77.00 776.00 779.00	736.00	* The units

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	ABLE

H607 310. 3291. 0.15300 0.014868 0.015551 1.774E 20				0.060 0.128 0.235 0.474	0.535 0.672 0.772 0.675	1.238	2.748 2.992 3.071 3.288 3.588	3.013 4.127 4.524 5.924 5.409	5.913 6.426 6.426 7.557 8.296	9.377 10.291 11.103 11.467
HG06 310. 3291. 0.030526 0.031267 1.925E 20				0.0000 0.1000 0.410	0.740 0.851 0.968 1.0968 1.239	1.5304 1.5527 1.6527 2.959	3.252 3.464 3.646 4.251	6.057 6.057 6.057 6.057	7.299 7.951 5.636 9.375	11,535 12,641 13,653 14,622 15,581
HG05 310. 3210. 0.03850 0.061842 0.062556 1.856E 20				66.232 6.3232 6.3232 6.3232	1.065 1.065 1.390 1.576	11.334 12.334 12.534 13.5344 13.534 13.534 13.534 13.534 13.534 13.534 13.534 13.534 13.5344 13.534 13.534 13.534 13.534 13.534 13.534 13.534 13.534 13.5344 13.534 13.534 13.534 13.534 13.534 13.534 13.534 13.534 13.5344 13.534 13.534 13.534 13.534 13.534 13.534 13.534 13.534 13.5344 13.534 13.5	4.095 4.529 4.619 6.973 5.392	5.097 7.0097 7.009 7.009 7.009 8.009	9-656 10-302 11-154 12-139	16.745 17.059 17.059 18.527 19.748
HG04 310. 1648. 0.03850 0.123684 0.125113		-		0.122	1.064 1.239 1.432 1.642	2.113 2.341 2.584 2.947 4.003	4.395 4.395 5.340 5.769	6.598 7.598 9.292 10.292	11.231 12.330 15.412 14.545 15.817	17.425 13.966 20.418 21.369 23.321
HG03 310. 1648. 0.01910 0.250109 1.854E 20				0. 0.1,73 0.368 1.9615	1.362 1.631 1.593 2.191 2.501	8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	5.905 6.260 6.726 7.306 7.995	6.504 9.738 10.791 11.929 13.149	14,445 15,769 17,124 19,525	21.4.7 23.591 25.255 26.985 28.695
HG02 310. 1645. 0.00977 0.498684 0.500146				0. 6.216 0.447 0.749 1.305	1.692 2.028 2.359 2.774 3.174	6 + + + + + + + + + + + + + + + + + + +	7.107 7.523 7.523 6.0031 6.017	10.703 11.850 13.127 14.494 15.938	17. 472 19.046 20.666 22.304 24.046	25.446 27.843 29.713 31.591 33.47
HC01 310. 1648. 0.00503 1.000000 1.001509				0.00 0 0.00 0.00 0.00 0 0.00 0.00 0.00 0 0.00 0 0.00 0 0.00 0 0.00 0 0.00 0 0.00 0 0.00 0 0.00 0 0.00 0 0.00 0 0.00 0 0.00 0 0.00 0 0.00 0 0.00 0 0.00 0 0.00 0 0.0	25.029 25.4629 35.4628 35.4628 35.4628 35.4628	2000 2000 2000 2000 2000 2000 2000 200	6.415 9.503 9.575 10.439	12.717 14.059 15.591 17.160	20.555 22.341 24.166 26.033 27.946	29.919
H706 310. 3291. 0.15300 0.029868 0.031239 3.563E 20	00.000000000000000000000000000000000000	0.1152 0.1152 0.252 0.3152 0.3153	0.567 0.568 0.681 0.782 0.998	1.039 1.173 1.324 1.535	2.10 2.10 2.10 2.10 2.10 2.10 3.10 3.10 3.10 3.10 3.10 3.10 3.10 3	4.22 4.45 4.45 4.41 6.41 6.41 6.41 6.41 6.41 6.41 6.41	5.413 6.439 7.239	7.520 8.455 9.161 9.938 10.776	11.676 12.590 13.533 14.534 15.690	17.204 19.914 21.190 22.459
HF05 310, 320, 0,08090 0,061053 0,06234, 3,851E 20	6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	0.071 0.115 0.181 0.254	0.555	1.091 1.259 1.449 1.700 2.231	2.502 2.725 3.225 3.229	2444 2444 2444 2444 2444 2444 2444 244	6.04 7.55 7.55 7.55 7.55 7.55 7.55 8.55 8.55	9.415 10.233 11.144 12.131 13.206	14,340 15,678 17,913 19,293	20.952 22.605 24.175 25.716 27.252
HF04 310. 3291. 0.03850 0.123684 0.125113	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.066 0.103 0.103 0.217 0.217	6.517 6.517 6.663 6.956	1.316 1.320 1.523 1.622 2.626	8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	4,359 5,719 5,009 7,699 7,699	7 .05 8 .05 9 .05 1 .05	11.070 12.079 13.201 14.407	17.064 19.436 19.842 21.292 22.669	24.701 26.482 28.236 29.976 31.715
HF03 310. 1643. 0,03850 0.247368 0,250226 3,718E 20	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	00.00 00.00 00.00 00.00 00.00 00.00	0.554 0.702 0.877 1.067 1.064	1.495 1.769 2.036 2.413	3.538 3.906 4.297 4.721	5.646 6.112 6.513 7.278	9.661 10.169 11.668	13.752 15.008 16.339 17.848	20,988 22,613 25,954 27,728	29.666 31.579 33.462 35.336 37.290
HF02 310. 1645. 0,01910 0,497368 0,500218		3 C C C C C C C C C C C C C C C C C C C	0.506 0.664 1.059	1.593	54.00 54.00 54.00 56.00 56.00 56.00 56.00	\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$	11.510 12.167 13.014 14.053	16.628 18.130 19.746 21.438 23.175	26.931 26.621 26.674 30.555	36.456 36.456 35.453 40.400 42.400
HF01 310. 1648. 0.09377 0.997368 1.000292	6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	0.15 0.20 0.20 0.20 0.20 0.30 1.30 1.30	7.566 0.713 1.146	1.770 2.168 2.628 3.197	6.4467 7.604 7.604 7.604 7.604 7.604 7.604	8.449 9.213 9.967 10.671	13.744 16.529 15.533 16.791 13.243	19-849 21-573 25-223 27-117	29.052 31.063 32.963 34.946	326.93 326.93 326.93 326.33 326.33
Sam. No. Temp (II) Path (cm) Conc. P (atm) Pc (atm) u (\$/cet)	(cm ⁻¹) 560-00 562-00 564-00 566-00	\$72.00 \$72.00 \$74.00 \$76.00	580.00 582.00 584.00 586.00	590.00 592.00 594.00 596.00 598.00	602.00 604.00 606.00 606.00	610 610 616 616 616 616 616 616 616 616	620.00 624.00 624.00 626.00	634.00 634.00 634.00 64.00 64.00	6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	658 658 658 658 656 656 656 656 656

13.367 14.104 15.070 15.939	19.976 19.978 20.637 21.660 22.494	23.305 24.114 24.696 25.639 26.314	27.054 27.735 23.412 23.974 29.473	29.932 30.359 30.769 31.125	31.69 32.166 32.466 32.466 5.69	32.934 33.723 33.995 34.100 34.211	34.542	35.152 35.152 35.465 35.467	35.534			
16.518 17.443 13.555 19.629 20.873	22.721 24.119 25.182 26.222 27.259	29.293 29.303 30.271 31.165 32.031	32.963 33.966 34.656 35.33 36.00	37.5564 37.664 37.664 39.009	39.000 39.000 39.000 39.600 39.600 39.600	60000000000000000000000000000000000000	42.027 42.134 42.322 42.468 42.68	\$20,400 \$40,000 \$40,000 \$40,000 \$40,000 \$40,000	43.643			
28.947 22.132 23.496 24.738 26.170	29.077 29.693 31.014 32.314 33.614	34.900 35.160 37.376 39.530	99999999999999999999999999999999999999	45.494 46.222 46.910 47.501 49.011	49.466 49.329 49.529 49.546	50.6642 51.6649 52.125 52.125	52.493 52.696 52.696 53.064	54.477 54.133 54.133 54.267 54.366	36.496			
24.763 26.179 27.702 29.163 30.718	32.656 34.460 36.646 37.584 39.055	40.562 42.068 44.6493 46.6493	47.617 49.999 50.221 51.132 52.435	53.393 55.393 55.193 55.964 56.624	57.216 57.737 58.199 59.630 53.995	59.790 60.951 61.358 61.554 61.769	62.039 62.239 62.400 62.718 62.952	63.212 63.613 64.9813 64.160	64.451	4./		
30.402 \$2.056 \$3.502 37.502	39.266 41.132 42.957 44.712 46.470	48.222 49.963 51.679 53.360 54.998	56.653 59.231 59.735 61.213 62.555	63.306 65.015 66.155 67.154 69.029	65.319 69.514 70.121 71.648 71.168	72.157 73.436 73.890 74.139 74.422	74.729 75.048 75.371 75.688 76.004	76.350 76.859 77.271 77.503	77.899			
35.364 37.235 39.112 40.972 42.985	44.000 46.000 46.700 50.695 52.613	56.531 56.443 58.349 60.234 62.033	63.949 65.775 67.519 69.198 70.812	72,356 73,849 75,258 76,516	79.654 79.557 60.347 91.025	92.763 84.169 84.704 85.013	45.775 86.197 86.627 97.056 87.40	85.500 89.500 89.847 89.371 89.656	99.946			
39.739 41.756 43.720 65.631 47.662	49.662 51.662 53.652 55.636	59.616 61.607 63.597 65.531 67.554	69.516 71.467 73.379 75.250 77.078	75.861 80.591 82.241 83.761	96.406 97.534 98.511 99.145	91.322 92.805 93.410 93.779 94.216	94.708 95.239 95.736 96.331 96.870	97.424 98.113 98.747 99.144	99.781			
23.707 24.939 26.366 27.749	31. 32. 32. 32. 35. 36. 36. 36. 36. 36. 36. 36. 36. 36. 36	39.201 39.505 40.764 41.969	655.50 65	49.236 50.002 50.750 51.391	52.431 53.874 53.265 53.613	54.801 55.853 56.203 56.403	56.854 57.074 57.239 57.500	57.986 58.414 58.765 58.914 59.054	59.195 59.133 59.671 59.611	59.465 59.465 66.037 66.109	600.265 601.309 601.367 601.417	69.512
28.770 30.270 31.946 33.520	37.150 39.003 40.624 42.215 43.608	45.363 46.937 48.455 49.929 51.342	52.307 54.262 55.563 56.821 57.945	58.973 59.969 60.926 61.759 62.473	63.116 63.695 64.208 64.660 65.124	66.018 67.257 67.723 67.968 69.236	68.797 68.797 69.078 69.355	69.972 70.498 70.925 71.114	71.451 71.511 71.760 71.902 72.052	72.166 72.254 72.336 72.411 72.474	72.523 72.563 72.597 72.625 72.655	72.682
33.162 35.162 36.944 38.729 48.529	66.266 66.266 66.266 69.064 69.004 69.004	51.535 53.338 55.063 56.767 59.425	60.106 61.776 63.322 64.793 66.161	67.443 68.688 69.887 78.940 71.854	72.684 73.432 76.092 74.670 75.261	76.314 77.684 79.241 79.554 78.554	79.237 79.598 79.956 80.297 80.647	81.049 81.656 82.171 82.419 82.635	200 200 200 200 200 200 200 200 200 200	6633 6633 6633 6633 6633 6633 6633 663	00000000000000000000000000000000000000	\$4.253
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44.061 46.340 48.320 50.30 52.301	54.301 56.30 56.30 50.234 62.272	64.260 66.249 65.233 70.215	74.167 76.123 78.953 81.790	93.559 85.380 87.110 88.705	91.532 92.773 93.571 94.627 95.755	97.150 98.717 99.435 99.926 100.468	101.052 101.659 102.259 102.871 103.475	104-121 104-959 105-706 106-158	106.925 107.256 107.850 108.03	108.711 109.345 109.455 109.549	109.650 109.743 108.749 108.928	109.901
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	H109 310- 3291- 0-15300 0-001684 0-001853 4-395£ 19		00000	6.151 0.179 0.211 0.244	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	2000 000 000 000 000 000 000 000 000 00	1.234	1.645 1.837 1.991 2.160 2.694	2.919 3.14 3.596 3.596 3.696
	M10k 310. 3291. 0.007632 0.007817 4.813E 19		00000 00000 000000 000000	0.195	0	1.009 1.059 1.117 1.113	1.455 1.555 1.556 1.723	2.00.3 2.611 2.611 2.617	## # # # # *** * * * * * * * * * * * * * * * * *
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JA dV	M102 310. 1648. 0.00250 0.50000 0.500375		00.000	40000000000000000000000000000000000000	0,500 0,500	3,220 3,529 3,529 4,604 4,604	5.124 5.124 5.124 5.144 7.244	9.065 6.975 9.943 10.977	13.579
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	инов 310. 3291. 0.038921 0.031278		0.056 0.056 0.127 0.205	0.572 0.572 0.661 0.756 0.356	11.10 11.10	25.55 25.55	3.452 3.6452 5.993 1.4644	5.236 5.145 6.149 6.149	3.446 9.277 10.011 15.777 11.412
	HHO) J10. 1648. 0.03F70 0.061842 0.062556		00000	000001	2.5.5.0	2.939	5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	6.50 7.465 7.465 9.659 9.659	011111 011111 011111111111111111111111
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	нисэ 310. 1648. 0.00977 0.249684 0.249413		9.244 9.244 9.742	1.397	1.937 2.320 2.520 2.616 3.577	4.23; 4.719 5.135 5.576	6.136 7.541 9.241 9.749	13.25 121.25 121.25 13.13.45 15.05 1	16.133 17.556 13.057 23.476 71.936
	HFG2 310. 1648. 0.03503 0.50303 0.5037.4		2000 2000 2000 2000 2000 2000 2000 200	1.597	2.510	0.250 0.250	2004 2004 2004 2004 2004 2004 2004	######################################	19.560 21.256 22.931 24.565 25.246
	HP01 310*16*46* 0.00250 1.000000 1.000750		**************************************	1.133 1.754 2.055 7.599	2.670 5.966 5.262 3.603 6.712	5,639 6,153 7,653 7,653	31196 30.245 11.633 10.245	13.666	22.331 26.0331 27.931 27.953
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66.77 7.79 7.79 7.79 7.60 7.60 7.60 7.60 7.60 7.60 7.60 7.60	11.0000 11.00000 11.0000 11.0000 11.0000 11.0000 11.0000 11.0000 11.0000 11.00	25.65 25.65	15-531 15-725 15-671 16-671	16.533 16.533 16.533 16.653 16.653 16.653	12.54 17.545 17.	17.576 17.625 17.675 17.724 17.772	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
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7.394 9.539 9.530 11.302 11.302	13.563	15.767	17.307	13.525	19-132	13.363	22.02 26.32 27.52 27.52 27.52 27.62 27.62 27.62
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15 /A	9291. 0.15300 0.001#95 0.001#85	, , , , , , , , , , , , , , , , , , ,	0.275 0.275 0.171 0.171	15.40	44.001 44.601 54.661	1221	355.52	3.55		22,12,4	11:000	******	******	5.175 6.219 6.219 6.219	
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	14402 3100- 1648- 0.00125 0.062500 0.06283							60000000000000000000000000000000000000	2.58 2.58 2.58 2.58 3.66 3.66 3.66	3.2 4.2 5.2					
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TABLE 17 JuAdu

HP09 310. 3291. 1.00000 0.096053 0.124868 7.488E 21	0.000 0.000 0.003 0.031	0.095 0.120 0.144 0.166 0.166	0.220 0.220 0.220 0.320 0.00 0.0		1. 572 1. 6572 1. 754 1. 363 1. 963 2. 134
HPO8 310. 3291. 0.15300 0.238158 0.249089	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.025 0.025 0.025 0.027	00.00000000000000000000000000000000000	7 00 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.032 0.0376 0.0926 0.996 1.064
HP07 310. 3291. 0.08090 0.488158 0.50005	0. 0. 0.000 0.000	0.021 0.025 0.025 0.028 0.032	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	4000	0.869 0.912 0.965 1.028 1.101
HP06 310. 3291. 1.00000 0.192105 0.249737 1.498E 22	9 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.136 0.177 0.212 0.254 0.317	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	. w.t.m.o.	33.156 33.4156 33.4499 33.721 33.971
HPO5 310. 3291. 0.15300 0.477632 0.499555 5.697E 21	0.006 0.006 0.012 0.014 0.025	0.046 0.054 0.066 0.077 0.095			1.570 1.654 1.745 1.851 1.979 2.129
HP04 310. 3291. 0.08090 0.976316 1.000011	0.007 0.007 0.025 0.040	0.072 0.093 0.111 0.114 0.124	0.163 0.231 0.231 0.272 0.317 0.369 0.427 0.482		1.722 1.798 1.890 2.004 2.140 2.306
HP03 310. 3291. 1.00000 0.385526 0.501184 3.006E 22	0.024 0.024 0.064 0.030	0.248 0.347 0.447 0.508	0.611 0.735 0.968 1.027 1.6027 1.585 1.764 1.942	7 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	5.037 5.037 5.690 6.105 6.105
HP02 310. 3291. 0.1530 0.955263 0.999110	0.024 0.024 0.052 0.075	0.190 0.219 0.254 0.302 0.363	0.427 0.576 0.576 0.666 0.774 1.110	66270	4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4
HP01 310. 3291. 1.000000 0.769737 1.000658 6.001E 22	0.037 0.107 0.138 0.222	0.655 0.582 0.694 0.633 1.025	2001 2001 2001 2001 3000 3000 3000 3000	2. 00. we to	6.741 9.327 9.999 10.771 11.623
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	2603 274. 1648. 0.01910 0.250109 2.098E 20				0000 TWONE TWONE ODDOO	11.469	22.1.22 2.12	50.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	######################################	12.00	20.376 22.154 23.659 25.659
	2601 274. 1648. 0.00500 1.001500 2.208E.20				00.114	1.527 1.900 2.306 3.747 3.207	4.5664 4.5544 5.4544 5.4544	72.00 20.00	12.733 12.050 13.443 14.945 16.546	18.256 70.05 21.405 25.742 25.742	27.646 29.631 31.647 33.676
	2704 274- 274- 3291- 0-029868 0-031239 4-031E 20		0.0346 0.1246 0.153	0.436	71.7	2000 2000 2000 2000 2000 2000 2000 200	2.5 2.5 2.5 2.5 2.5 2.5 2.5 3.5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	50000 50000 50000 50000 50000	6.051 7.567 7.567 7.567 7.051	10.721	15.215 16.627 17.953 19.243
	2704 274- 274- 3291- 0.03850 0.123684 0.125113	3. 0.032 0.017 0.036	0.0000	0.276	######################################	2.152	3.665 3.666 3.666 3.666 3.77	6.44 7.66 7.66 7.66 7.66 7.66 7.66 7.66	9.050	16.536 15.336 17.341 10.312	22.164 23.991 25.746 27.526 29.316
L'Adv	2702 274- 1648- 0.01910 0.498684 0.501542	00.004	0.0354	00000	0 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	74.44 01.04 01.04 01.06 00.00 00.00	5.561 6.093 7.267 7.267	9.663 10.233 10.931 11.913	14:449 20:593 14:449 20:593	22.391 26.101 26.101 28.012	33.940 33.9340 35.939 37.938
4.7 6	2E05 274. 3291. 0.15300 0.059737 0.062479	0.002	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.00 0.10 0.00 0.00 0.00 0.00 0.00 0.00	11.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00	2.667 2.049 3.046 3.046 3.046	6.50 6.50 6.50 6.50 6.50 6.50 6.50 6.50	7.690 6.109 6.604 9.826 9.961	10.434 21.434 21.434 21.434 21.434 21.434 21.434	16.840 19.751 19.753 21.302 22.927	26.77d 25.677 26.146 30.773 32.103
TABLE 1	ZE03 274. 3291. 0.03850 0.247368 0.250226	3 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	9.075 0.111 0.151 0.214	0.561 0.745 0.947	1.172	6.036 6.036 6.036 6.036	6.710 7.32~ 7.943 8.711	11.349	15.412 17.939 19.529 21.224 22.73	24.435 25.701 23.525 37.525	36.463 36.463 59.461 40.461
TAE	2E01 274. 1648. 0.01910 0.994737 1.000437 8.392E 20	30 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.370 0.130 0.139 0.139 0.245	0.391	2.756 2.567 2.547 3.547 5.580	5.00 mm m	10.063 11.061 12.051 13.149	16.239 17.235 13.546 24.546 21.740	23.503 25.430 27.430 23.430 31.440	\$2000 \$2000	43.439 49.339 47.439 49.339 51.339
	2704 8'44- 0-182833 0-185833 0-185831-0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	000000000000000000000000000000000000000	0.663 0.867 1.117 1.373	7.00 7.10 7.10 7.10 7.10 7.10 7.10 7.10	4.380 5.381 5.966 6.601	8.017 8.719 9.440 10.341	14.00 14.745 15.019 17.025	18.429 20.054 21.731 23.474 25.787	27.159 29.039 30.953 32.695 34.495	00000000000000000000000000000000000000
	2002 274- 3291- 0.03650 0.494737 0.500451	00.00	0 1169	1.064 1.397 1.772 2.213	2.736 3.519 3.975 4.761 5.950	6.902 7.794 9.759 9.759	11.992 13.103 14.221 15.474 17.261	14.611 19.959 21.102 22.859 24.619	26.490 78.421 30.379 32.357 34.346	246.944 246.944 246.944 246.544 246.44	666. 666. 666. 666. 666. 666. 666. 666
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	2C01 874- 3291- 0.03650 0.988156 0.999531	00000000000000000000000000000000000000	000000000000000000000000000000000000000	2,1295 2,1295 2,1564 2,1662 2,1662	5.225 4.225 4.426 19.764	111.46 113.46 15.002 16.654 13.450	20.057 21.172 23.500 25.300	29.154 30.455 32.677 34.613 16.597	33.536 42.536 42.539 44.536	63,596 50,596 52,596 56,596 56,596	58.596 62.596 62.596 64.596 66.596
	ZBGE 274. 3291. 0.15300 0.477632 0.499555	00000000000000000000000000000000000000	**************************************	2.703 7.449 6.1261 6.061	7.165 9.537 9.615 11.0043	14.461 16.042 17.301 19.419	22.936 26.622 26.522 20.502 30.502	32.163	41.360 45.960 47.960 47.960 49.960	51.960 53.960 55.960 57.960 59.960	61.950 63.960 65.960 67.960 69.960
	2A01 #74. 3291. 0.15300 0.956379 1.000486	7449 7449 00000	44 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	4.997 6.205 7.6705 7.675 8.976 10.519	12.172 13.910 15.726 17.626 19.616	21.567 23.551 25.532 27.526 29.525	35.555 35.555 35.555 37.555 37.555	11.525 13.525 15.525 17.525 19.525	51.525 53.525 55.525 57.525 59.525	61.525 63.525 65.525 67.525 69.525	71.525 73.525 75.525 77.525
	Sam. No. Temp (X) Fath (cm) Conc. Fath (cm) Fath (cm) I (dtm) L (\$\psi(\cup \text{c}	(cm ²) 262.00 562.00 565.00 566.00	572,40 572,40 574,400 576,400	9996 996,000 996,000 996,000	596.00 594.00 596.00 596.00	602.00 602.00 604.00 606.00	610.00 612.00 614.00 616.00	622.00 622.00 624.00 626.00	630.00 632.00 634.00 635.00	640.00 642.00 642.00 645.00	655.00 654.00 655.00 655.00

11 736 13 479 15 515 17 515 17 515 17 515 18 517 18	21.675 23.483 23.952 23.952 25.955 25.925 25.925 26.484 27.744	29.167 29.167 29.167 29.163 29.163 29.163 29.627 29.627	300.729, 300.729, 310.934 311.36 311.363 311.363 311.363	31.664 31.805 31.905 32.034 32.090		
2000 00 00 00 00 00 00 00 00 00 00 00 00	15. 15. 15. 15. 15. 15. 15. 15. 15. 15.	6652 67.7552 67.7552 67.7552 66.77552 66.77552 66.77552 66.77552 66.77552 66.7752 66.7	50000000000000000000000000000000000000	52.0443 52.0443 52.284 52.284 52.490 52.490		
29.203 30.961 30.961 36.518 36	647.537 52.6327 52.6327 52.6327 56.5137 56.656 61.966 61.966	65.208 65.308 66.190 (6.190 67.627 63.7216 69.163	70°424 71°504 71°504 72°195 72°71 72°71 72°71 72°71 72°71 73	74.517 74.655 74.655 75.059 75.275		
13.655 13.655 13.655 13.655 14.657 14.627 55.6627 56.627	57.627 (3.627 (3.627 (5.627 (5.627 (5.627 (5.627 (6.627 (7	735.556 827.756 827.756 847.650 847.744 847.650 86.256	67.626 69.210 69.210 90.434 91.324 91.324 91.806	947213 947213 94.5513 94.5513 94.5613		
21.152 26.043 26.043 26.043 27.569 31.158 32.560 31.560 31.560 31.560 31.560 31.560	130 130 130 130 130 130 130 130 130 130	64.435 64	52.116 53.116 53.106 53.5609 54.5609 56.717 56.717 56.717	55.003 55.003 55.003 55.003 55.003 55.003 56.003 50.003	56.33 56.33 56.33 56.53 56.65 56.65 56.65 56.65 56.73 56.73 56.73	56.755 56.772 56.780 56.781
321. 36.5461 36.5461 4	6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	65.647 67.727 67.727 69.660 69.660 70.117 71.365 71.365	73.137 74.412 74.412 75.134 75.134 75.134 76.136 76.370 76.360	77.305 77.751 78.154 78.422 78.422 78.422	79.5167 79.5267 79.5424 79.6424 79.6644 79.6647	79-712
4,1,92,4 4,1,92,4 4,1,916 4,1,	61.911 65.911 67.911 71.89 75.73 79.693	62.984 86.611 86.611 87.400 87.400 89.679 91.428	93.368	99.635 100.302 101.300 101.300 101.913	102.635 102.786 102.926 102.927 103.019	103.139
23.00.00 24.00.00 24.00.00 25.00.00 25.00.00 25.00.00 25.00.00 25.00.00 25.00.00 25.00.00 25.00.00 25.00.00 25.00.00 25.00.00	55.00 50	72.579 72.579 73.579 74.666 74.666 76.665 76.665	77.617 79.75 79.77 79.77 80.06.06.06.06.06.06.06.06.06.06.06.06.06	6666 6666 6666 6666 6666 6666 6666 6666 6666	24 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	95.24 95.24 85.294 85.343 85.343
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63.139 57.350 57.359 61.359 65.359 65.359 67.359	77. 75. 77. 77. 77. 77. 77. 77. 77. 77.	195.45 195.45 195.45 195.45 195.45 195.65 195.65 195.65 195.65	1112.115.115.115.115.115.115.115.115.115	120.745 121.454 122.917 123.644 124.519 124.519	125.052 126.221 126.521 125.622 125.622 125.632 126.632	127.020
4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	(6.34 72.44 72.44 74.44 74.44 76.43 76.43 76.43 84.46 84.43	94.104 99.404 91.407 91.407 94.11.3 96.349 96.339	101.3.46 101.3.46 102.2.3.8 102.2.3.8 102.2.3.8 102.0.3.8 105.3.8 106.667	103.241 103.054 103.054 103.054 110.245	111.555 111.555 111.955 111.951 112.116 112.559 112.559	112.766
\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$	776 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	90.349 90.349 100.326 104.169 107.275 109.371 110.526	115.902 115.715 115.894 116.894 119.872 120.897 121.957	1255.149 1265.343 1275.5343 1286.341 1286.341 1296.626	131-139 131-139 131-139 132-139 132-139 132-139 132-139 132-139 133-13	132.652
66.15 6.15 6.15 6.15 6.15 6.15 6.15 6.15	81.5.5.4 84.5.49 84.5.49 84.6.69 84.69 85.60 85.	101-939 105-930 105-930 107-670 111-670 111-670 111-670 111-670	113, 924 113, 785 113, 785 113	130.274 131.256 132.330 133.711 134.711 135.136	164-449 164-449 164-449 164-449 164-449 164-449 164-449 164-469 164-72	139-401 139-401 139-479
17.7.1.2 17.7.1.2 17.7.1.2 17.7.1.3 17.7.1	\$4.000	1105:546 1117:556 1117:556 1117:556 1117:556 1120:545 1120:545	2000 000 000 000 000 000 000 000 000 00	11.00.000	155.05 5 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	157.751
71.95.7 72.96.7 72.96.7 72.96.0 72.96.0 75.96.0 75.96.0 75.96.0	91.568 93.968 95.468 95.468 99.968 101.968 105.968 107.968	1111-960 1115-960 1117-960 1117-960 1121-960 1121-960 1121-960 1125-912	137.745 137.745 137.745 137.745 137.745 144.045 144.045 144.045 144.045 144.045 144.045	1557. 1578 1557. 1578 1557. 1578 1557. 1578 1576. 1578 1576. 1578	169.44	163.969
111 64 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	101 102 103 103 103 103 103 103 103 103 103 103	\$25.681 \$25.88	141.5523 143.5523 143.5523 143.5523 151.683 155.683 155.683 155.683 155.683 155.683	161.634 165.463 167.174 159.225 171.010	177:176:176:176:176:176:176:176:176:176:	162.996 193.003 183.590 183.696
6 6 7 4 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	200 - 100 -	2000 1000 1000 1000 1000 1000 1000 1000	00 * F Z 00 * S	745.00 745.00 745.00 745.00 745.00 745.00	751.00 751.00 751.00 762.00 765.00 765.00 775.00	77-50 776-03 774-83 770-03

The units of u are molecuies/cm2, abbreviated here by (θ/cm^2) .

	ZJIO 874. 3691. 0.15300 0.001868 0.001954				0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.219 0.234 0.251 0.273	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	0.554 0.624 0.624 0.624	100112 10012 100261 10458	968. 916.11 968. 97. 97. 97. 97. 97. 97. 97. 97. 97. 97
	2.08 274- 3291- 0-03850 0-007763 0-007853				0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	00 00 00 00 00 00 00 00 00 00 00 00 00	00000 00000 00000 00000	11.126	1.937 2.286 2.602 2.502	######################################
	2.104 2.74• 2.44• 1.446• 0.01910 0.031053 0.031231				000000000000000000000000000000000000000	0.661 8.660 0.732 0.739	1.092 1.092 1.183 1.183	1.760 1.980 2.5215 2.677	7.062 4.062 4.063 4.063 4.063	5.447 6.199 6.548
	2.04 8.74. 16.48. 0.00500 0.12500 0.125188				0.05 0.111 0.132 0.571	10077 10077 10077 10077	1.631	2.778 3.155 3.557 4.557 4.557	7 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	6.837 9.434 18.197 18.756 11.694
	2.002 274- 274- 1646- 0.00125 0.500000 0.500188				0.0 0.0 0.13? 0.210 611	10000 10000	1.650 2.239 2.635 3.101	5.669 5.669 5.669	7.667 6.765 9.835 10.921	13-124 15-170 15-203 16-187 17-346
	2.301 E74. B26. 0.00125 1.000075 2.767E. 19				0.069 0.137 0.516	11, 11, 12, 12, 13, 13, 14, 15, 15, 15, 15, 15, 15, 15, 15, 15, 15	1.0000 1.00000 1.00000 1.00000 1.00000 1.00000 1.00000 1.00000 1.00000 1.000000 1.00000 1.00000 1.00000 1.00000 1.00000 1.00000 1.00000 1.00000 1.00000 1.00000 1.00000 1.0000000 1.00000 1.00000 1.00000 1.000000 1.000000 1.00000 1.00000 1.00000 1.00000000	5.055 5.732 6.712 7.014	9.156 11.765 13.104	17-1892 17-1892 18-134 29-465 28-976
αþ	2109 274- 3291- 0-003684 0-003683 4-972E 19		**************************************	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.1130 0.1150 0.2120 0.374	00000 00000 00000 00000	0.716 0.771 0.639 1.010	1.13	22.52.6	2000 A 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4
A 7	2107 274- 3291- 0-03850 0-015395 0-015573		0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	0.190	9.375 0.459 0.528 0.528	1.003	1.531	2.235	7 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 -	6.0446 7.0446 8.0446 8.055
TABLE 20	2105 274. 1646. 0.01910 0.062105 5.239E. 19 :	ł	0.354 0.154 0.154 0.262	00.000	0.725	1.951 2.951 2.206 2.308	2.565 2.523 3.108 3.737 3.737	**************************************	7.126 7.929 8.631 9.345	10.777 11.473 12.314 12.990
TA	2103 274. 1648. 0.00540. 0.25000 0.250375		0.069 0.140 0.214	0.0000000000000000000000000000000000000	1.039 1.157 1.271 2.003	2.533	3.572	6.903 7.663 8.533 9.508	10.776 11.993 15.135 14.315	16.723 17.882 19.079 26.138 21.459
	Z131 274. 1648. 0.00125 1.00000 1.000375 5.521E 19		60.00 60.00	0.460 0.710 0.862	1.517 1.5436 2.5636 2.563	2.850 3.124 3.354 3.653	**************************************	7.805 8.906 10.119 11.436 12.869	16.503 16.159 17.796 19.464 21.148	22.628 26.669 26.879 27.619
	ZHOS 274- 3291- 0-15300- 0-007540 0-007844		000000000000000000000000000000000000000	0.235	0.520 0.570 0.659 0.976	10.23	1.716 2.022 2.207 2.207	2.650 2.983 3.170 3.465	2242	7.653 7.653 7.673 8.155
	2N06 274- 3291- 0.03850 0.030921 0.031278		00.000	00000 10000 10000 10000 10000	0.994 0.994 1.185 1.687	2.179 2.179 2.308 7.67	2.876 3.133 3.627 3.766 4.149	6.026 5.026 5.598 6.041 6.742	7.704 8.565 9.309 10.051	11.532 12.261 13.191 13.933 15.000
	2904 274- 1648- 0-01910 0-124342 0-125055		0.000 0.254 0.253	0.566 0.795 1.668	1.203	2.925 3.073 3.276 3.540	6.237 5.203 5.799 6.466	7.288 7.976 8.812 9.718	12.146 13.409 14.681 15.821 17.863	15.291 19.495 28.810 21.969 23.438
	2H02 274. 1448. 0.00500. 0.500000 0.5000750		0000 0000 0000 0000 0000 0000	0.792 1.192 1.603 1.603	1.885 2.107 2.322 2.565 3.414	6.531 6.531 5.937 5.936 5.936	6.100 6.827 7.673 9.619 9.656	10.796 12.030 13.342 14.737	17.958 19.701 21.403 23.136 24.891	26.647 28.378 38.186 31.784 33.693
	Sam. No. Temp (K) Path (cn) Conc. P (atm) U (\$\psi(\text{cm})\$) U (\$\psi(\text{cm})\$)	(ca.'.1)	610.00 617.00 616.00 616.00	00°929 90°929 90°929 90°929	630.00 632.00 636.00 636.00	**************************************	650.00 652.00 654.00 656.00 656.00	6660.00 666.00 666.00 666.00 666.00	674.03 672.00 674.00 676.00 675.00	666 667.00 667.00 666.00 686.00

	2100£ 274. 1648. 0.00125 0.031316 0.031318						0.161 0.235 0.317 0.377	1.5611						
	ZM01 274- 8E4- 0.06125 0.062500 0.062503					 0 - 3 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	0 - 219 0 - 471 0 - 571 0 - 571 0 - 571	1.767 1.959 2.224 7.352 7.352	2 + 9 2					
	2004 274- 1648- 0-00500 0-015658 0-015681					0.036	20000	1.25	2.191					
	ZMOR B74. 1646. 0.00185 0.068503 0.068523					0.16	0.136 9.693 9.057 0.763 1.244	2.22 2.25 2.25 2.25 2.25 2.25 2.25	3.4.20					
	2401 874- 824- 0-00125 0-125000 0-125047 3-459£ 18					9.513	10001	2.665 7.100 7.125 7.561	4.054			_		
	2108 274- 3291- 0-03850 0-001895 0-001917	38 C 8 0	\$ 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	00 00 00 00 00 00 00 00 00 00 00 00 00	2000 2000 2000 2000 2000 2000	# 00 # 0	44.00	2.4.4.4.4.4.4.4.4.4.4.4.4.4.4.4.4.4.4.4	100.1 200.2 200.2 200.2	22.22	2.330	2.417. 2.417. 2.417. 2.417.	2000 2000 2000 2000 2000 2000 2000 200	22.22
LA du	24.5. 2.4.5. 2.4.5. 2.4.5. 2.4.5. 2.4.5. 3.4	 	00.11.00	0.219 0.271 0.271 0.100 0.440	000000 00000 00000 00000	10.11 10.11 10.11 10.11 10.11 10.11	1.275	2.727 2.933 3.946 3.245 3.245	2.25. 2.44. 2.44. 2.44. 2.44. 2.44. 3.44.	3.44.		1,243 1,243	20000	*****
21	2104 874- 1448- 0-00500- 0-031314 0-031344 6-916E 18	0.00 0.00 0.00 0.00 0.00 0.00		9.521 9.544 9.731 0.123	0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	2000 2000 2000 2000 2000 2000 2000 200	2,712 2,000 3,265 3,265 3,265	50.00 50.00	4.00 4.00 4.00 4.00 4.00 4.00 4.00 4.00	\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$	7.577	7.445	3.00 4.00 5.00 5.00 5.00 5.00 5.00 5.00 5	3.224
TABLE	2LOE E74- 1648- 0.001E5- 0.129000 0.129047	00.00	00.00 00	2000 2000 2000 2000 2000 2000 2000		22.22.22.22.22.22.22.22.22.22.22.22.22.	3.773 4.3663 4.5654 5.7358	7.566	3.606 9.406 9.407 9.674		11.152	11.696	12.033	12.284
	2L01 874- 0.00125 0.250000 0.850094 6.918F 18	2000 6000 6000 6000 6000 6000 6000 6000	00000 00000 00000	2000 2000 2000 2000 2000 2000 2000 200	1.0173	2.722 1.5159 1.9564 1.4159	565.5 5.55.5 5.55.5 5.55.5 5.55.5		10.71.	15.439 15.175 15.421 15.725 13.949	11.793	111111111111111111111111111111111111111	16-195 15-192 15-263 15-263 15-296	15.304
	2X08 274- 3891- 0.03890 0.003816 0.003860	00.00	**************************************	0.759 0.754 0.754 0.327	0.00 0.11 0.554 0.554 0.554	2000 1000 1000 1000 1000 1000 1000 1000	3,55,1 1,514 1,694 1,694	0000 0000 0000 0000 0000 0000 0000 0000 0000	8	3.968 1.1559 1.1559	1,261	******	1,555 1,555 1,6537 1,6693	1111
	2006 E74. 1646. 0.01910. 0.015386 0.015415	7.00 7.00 7.00 9.01 8.01 8.01	*****	7.572 9.673 9.573 9.575 9.575	1.935	1.7.1 7.00.1 7.00.7 7.00.5 7.00.5	7.466 7.456 7.456 7.456 7.456 7.456 7.456	0.00 th	44.54 64.54 64.64	7.295	7.17.77.77.913.4	497.4 497.4 497.4 497.4	**************************************	4.676 4.746
	ZKG4 E74- 1646- 0.00500 0.042500 0.062594 1.380E 19	2000 2000 2000 2000 2000 2000 2000 200	0000 00000 00000 00000	0.000 0.000 0.000 0.000 0.000 0.000	2,0017		2014 2014 2014 2014 2014 2014 2014 2014	2000 2000 2000 2000 2000 2000 2000 200	10.505	951-21 15-21 551-21 551-21	12.939	13.550	11.11.2	14.356
	ZKOE #74- 1646- 0.001#5 0.850000 0.850094- 1.380E 19	0 - 1 - 0 - 0 - 0 - 0 - 0 - 0 - 0 - 0 -	0 6 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	8	2.64.7	21007 21007 21007 21007	7	11.23	1000 1000 1000 1000 1000 1000 1000 100	14-11.7	20.05 20.05	20.917. 21.109 21.109 21.109	21.13 21.13	21.934
	2x01 234. 824. 0.500025 0.500185 1.384E 19		\$	04444444444444444444444444444444444444	2.5.06 2.6.05 3.6.64 3.6.64 4.6.64	2,165,7 2,165,7 2,165,7 4,165,7	9.005	13.513 15.563 15.663 17.573	23,256	22,433 23,069 23,636 24,536 24,536 24,554	\$555 \$555 \$555 \$555 \$555 \$555 \$555 \$55	25.991 26.163 26.163 26.223 26.223	25.45. 25.45. 26.45. 27.55. 27	27.156 27.156 27.155 27.173
	Sau. No. Temp (R) Path (ca) Conc. P (ata) U (\$/cm*)	 37900 0000 0000 0000 0000 0000 0000 0000	\$25.00 \$25.00 \$25.00 \$25.00 \$25.00	510 617 617 617 617 617 617 617	\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$	\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$	6651.666 6651.666 6651.666 6651.666	570.80 677.80 671.90 675.00	6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	690.00 697.00 697.00 697.00 697.00	000 00 00 00 00 00 00 00 00 00 00 00 00	717.	770.33	752.03 752.03 754.03 756.03

		i																							
	2004 274- 2291- 1-00000 0-192103 0-24737		6.198 8.371	8.63B	1.074	2.186	2,2,2	2,533	2.688	2.985	3.120	0 kg kg	3.568	3.636	3.698	3,786	3,885	3,922	3.942	3.994	4.011	151	27.8.4	9	4.114
	Z605 274- 3291- 0-15300 0-479555 6-446F E1		8.163 8.195	6.338	8.413 0.689		1.433	1.528	1.703	1.886	1.966	2-118	2.238	2,293	2.341	2.410	2.4.87	2.525	2.552	2.586	2.616	2.568	2.685	7.01	2.740
4 d 2	2004 E74. 3E91. 0.08090 0.976316 1.000011		8 - 113 8 - 208	8.293	1.437	1.236	1.519	1.608	986	200.2	668.3	2.275	2.347	2.467	2.514	965-2	07007	٠.	2.739	: ~	•	••	2.636	σ,	2.943
23 /	2003 E74 3291. 1.00000 0.364211 3.3695		8. 8.388 8.728	1.807	1.647	2,901	3,663	3.955	6.537	5.121	5.386	5.656	6.230	6.375	6.491	6.660	658.9	6.936	6.986	7.062	7.102	7.139	7.216	1.259	7.304
TABLE	2002 E74- 3E91- 0-15300 0-956579 1-000-866- 1-291E RE		6.207 6.392	8.673	1.275	1.918	2,375	2.533	80	3.235	3.400	7.67	3,745	3.964	6.036	**************************************	1.25	4.301	4.340	4.196	4.427	404.4	4.536	• 566	4.554
-	Z001 874- 3291- 1-00000 0-769737 1-000658		8.762 1.434	2.513	3.722	5.847	6.375	6.916	8.063	9.19	9.712		11.823	11.639	11.659	12.176	12.524	1 (1)	12.723	15.841	12.901	256.31	13.056	13.113	13.168
	Sam. No. Temp (K) Path (cm) Conc. F (atm) P (atm) U (\$/cm')*	, (1.8)	760.68 762.00 754.00	786.80	790.00	794.80	796.88	806.80	000,000	989-88	610.80		516.60 618.00	828.00	622.00	826.80		932.00	834.00	638.60	940-60	942-00	366.00	848-08	850.00
							=		_			=	_		_	_		_	ż	_		_	-	=	
	ZP06 274- 3291- 1.00000 0.198105 0.269737		9'22' 10 0 0 0 0 0 0 0	8.065	6.107	0.128 0.144	1.176	8.211 8.246	8.288	9.395	44.0	5256	8.664 8.652	169.8	6.731	1.00		1.939	2.040	2.369	2.458				
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Adz	ZPOS E74- 3E91- 0-15300 0-47453 6-446E E1			::			•	101	0.836	250.0	0.070	160.0	3 2	0.153	171.		9-76	.893 8.805	0.052	8-975	45			hy (6 /m ²)	c o) (*/cm /.
22 /4	27, ZPO4 ZPO5 274, 2291, 3291, 3291, 0.08090 0.15300 0.974316 0.49553 1.000011 0.495553	_			•••			8.611 8.661 8.867	1669 8-842 8-819 166 8-857 8-819	6.83 6.878 8.852	0.070	951-8	8.191 8.136	8.213 0.153	8.237 8.171	0.00	347.0	90000 8 8600	0.052	2.500 B 201.1	.176 1.845	-		hyperistad have hy (# /cm²)	orevaled sere of (*/cm).
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	1605 245: 3591: 0.03830 0.041848 0.048384	-				8.467 8.144 8.235 8.235	4.55 4.55 4.45 4.45 4.45 4.45	10 10 10 10 10 10 10 10 10 10 10 10 10 1	2000 2000 2000 2000 2000 2000 2000 200	5 4 4 6 5 2 4 4 6 5 2	7.104	12.423 13.718 15.008 16.027 17.666
	1863 1644- 0-01910 0-256109 2-3562						0.792 0.987 1.281 1.625 1.662	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	6.251 6.677 6.883 5.231	6.399 7.140 8.084 8.975	11.235 12.513 13.687 15.349	18-654 28-471 22-245 24-853 25-863 25-863
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	0.15300 0.0079868 0.0079868 0.0079868		•••••	12.000	497.8 497.8 171.8 6119		1.161	2.0317 2.0317 2.051 3.0517 3.0517	44.00 46.00 46.00 46.00 46.00 46.00 46.00 46.00 46.00 46.00 46.00 46.00	50 41 40 60 41 40 60 41 40 60 41 41 40 60 41 41 41 41 41 41 41 41 41 41 41 41 41	8-458 9-299 10-228 11-241 12-361	13.613 15.251 16.594 17.952 19.347
	LF04 E44- 3291- 0-03650 0-123684 0-125113 4-717E 80		••••		0.025 0.127 0.127 0.127 0.347		1.0651 1.0653 1.0653 2.0156 2.056	2.982 3.2982 4.554 511	5.645 5.645 6.5819 6.585	7-776 9-579 9-513 10-560	12.988 14.328 17.75 18.855	20.62 22.507 24.310 26.147 27.998
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	LEO3 E44. 3291. 0.03650 0.247368 0.250226			0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	00 00 00 00 00 00 00 00 00 00 00 00 00	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		5.236 6.314 6.926	9.00 mm	13.842 15.229 16.755 18.384 20.181	21.911 23.763 25.664 27.686 29.566	41. 43. 43. 43. 43. 43. 43. 43. 43
TABLE	LEG1 244- 1646- 0-01910 0-994737 1-000437		00.00 0.00 0.00 0.00 0.00 0.00 0.00 0.	00000000000000000000000000000000000000	6.557 6.725 9.725	400 400 400 400 400 400 400 400 400 400	5.13 5.72 5.72 7.53 7.53 7.53 7.53 7.53 7.53 7.53 7.53	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	14.099 16.978 17.626 13.997	20.732 22.569 24.671 26.412 28.382	200 200 200 200 200 200 200 200 200 200	## ## ## ## ## ## ## ## ## ## ## ## ##
·	LD04 E44- 0-15300 0-119737 0-125233 1-615E 21			0.119 0.162 0.277 0.376	8.524 6.524 6.994 1.228	2	6 4 4 4 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	6.641 7.272 7.984 7.984 10.8629	11.242 11.910 12.719 13.707	16-172 17-640 19-245 20-935 22-715	24-536- 26-451 26-451 36-375 32-334 32-334	36.296 36.296 38.296 40.296 42.296
	LD02 844- 3291- 0-03850 0-454737 0-500451				0.550 0.750 0.992	2.017 2.017 2.060 3.260 4.250	8.00 9.00 9.00 9.00 9.00 9.00 9.00 9.00	9.663 11.667 11.7753 14.7753	15.906 18.938 18.178 19.629 21.282	24.9863 26.934 26.913 28.679 38.666	32 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3	
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	LCO1 847- 3891- 0-03830 0-988158 0-999571 3-788E R1		000000000000000000000000000000000000000	0.1150	2.051 2.051 2.055 2.055 2.055 2.055	5.4.26 5.2.39 5.2.33 6.487	9.331 10.727 12.210 13.764 15.377	17.012 18.652 20.297 21.992 23.921	25.886 27.436 29.199 31.183	35.076 37.876 39.876 61.076	45.876 47.876 49.076 51.876 53.076	55.876 57.846 59.876 61.076 63.876
	LB0E R46. 3291. 0.15300 0.47763E 7.128E E1		# .059 # .120 # .120 0 .269	0 . 3 6 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	5.167 6.163 2.203 6.569	11.662 13.151 14.728 16.376 16.095	19.837 21.596 25.348 25.161 27.125	29.0 42 30.749 32.559 36.466	38-671 60-671 62-671 66-671 66-671	63-671 50-671 56-671 56-671	58.471 60.471 62.471 64.471 66.471
	LA01 246. 3291. 0.15300 0.956579 1.000466			2 + 6 + 6 + 6 + 6 + 6 + 6 + 6 + 6 + 6 +	2000 400 400 400 400 400 400 400 400 400	8	17.794 19.731 21.693 23.674 25.662	27.661 29.661 31.661 33.661	37.668 39.654 41.654 43.654 45.654	159.85 159.85 159.85 159.85	57.654 53.654 61.654 63.654	69.656 71.656 73.656 75.656
	Sam. No. Temp (K) Fath (cm) Conc. P (Atm) P (Atm) P (Atm) U (\$ (cm))*	, (E)	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	570.80 572.60 574.80 575.80	50 00 00 00 00 00 00 00 00 00 00 00 00 0	5990 5990 5996 5996 5990 5990 5990 5990	2000 2000 2000 2000 2000 2000 2000 200	612.40 612.40 614.00 616.00 618.00	628.00 622.00 624.00 626.00 628.00	632.00 632.00 634.00 636.00		6550.00 655.00 656.00 656.00 659.00

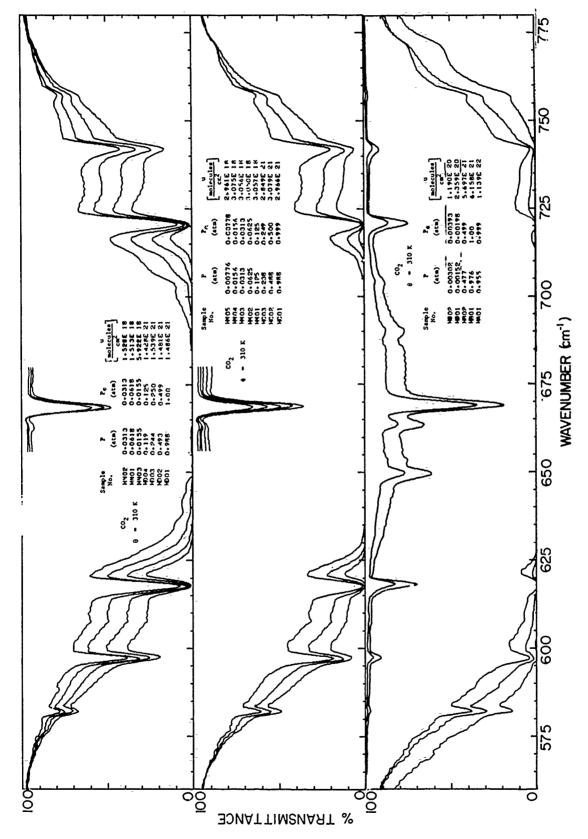
11.167 11.955 12.968 13.986 14.977	16.731 17.973 18.858 19.743 21.633	21°51° 22°35° 23°91° 23°91° 20°52°	25.242 25.423 26.423 26.922 27.315	27.983 28.278 28.278 28.588	28.861 29.884 29.131 29.245 29.358	29.686 38.289 38.437 30.493 38.565	38.686 38.748 38.765 36.855 36.926	31.800 31.115 31.218 31.294 31.836	31.301			
19.036 20.359 21.986 23.239 24.788	26.719 26.369 29.779 31.193	34.822 35.482 36.725 37.974 39.142	62.238 62.295 63.295 63.166	64.682 45.195 45.726 46.181 66.557		68.262 69.167 69.682 69.535	59.901 59.905 58.205 51.236	500 500 500 500 500 500 500 500 500 500	51.144			
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28.73. 23.5982 23.5982 25.127 26.112	26.648 38.343 31.798 33.247	36.138 37.548 38.998 48.198	42.561 43.668 44.698 45.602 65.411	47.112 47.736 68.389 68.888	49.569 49.888 58.158 58.588	51.044 51.972 52.334 52.452	52.738 52.698 53.043 53.191	53.45 53.76 53.94 54.652 54.14	54.223 54.296 54.368 54.415	54.598 54.541 54.572 54.593	24.65.65 5.65.	54.655
29 20 20 20 20 20 20 20 20 20 20 20 20 20	39.374 61.333 65.052 66.052	68.841 52.547 54.352 56.352	57.887 59.649 68.973 62.399 63.708	64.888 65.969 66.952 67.689	69.147 69.691 70.162 70.567	71.626 72.622 73.265 73.461	73.950 74.219 74.455 74.763 75.021	75.277 75.615 75.951 76.137	76.432 76.551 76.655 76.762	76.67 76.911 76.952 76.990 77.019	77.835 77.036 77.036 77.835	77.038
33 - 2 - 2 - 2 - 2 - 2 - 2 - 2 - 2 - 2 -	49.282 51.282 53.282 55.282 57.282	53.282 61.282 63.282 65.282	69.271 71.240 73.174 75.853 76.663	78.596 58.246 81.783 85.148	85.389 85.327 87.148 87.534 85.444	99.34 98.85 98.423 98.75 92.453	92.599 92.599 92.599 97.999 97.999	96666666666666666666666666666666666666	96.778 96.957 97.091 97.193	97.328 97.372 97.487 97.432	94.70 94.70 94.40 94.40 94.40 84.40	947.16
34.76 34.76 35.65 37.96 37.96 37.96 37.96 37.96	612.64 67.622 67.622 67.622 67.622	51.114 52.999 54.867 56.700 58.486	64.231 61.938 63.595 66.979 66.331	67.551 68.679 69.727 78.638	72.658 72.652 73.176 73.626	74.772 76.627 76.874 77.149	77.448 77.759 78.672 78.388	78.961 79.869 79.796 88.887	38	81.052 81.052 81.153 81.123	91.223 91.223 91.264 91.266	31.311
41.559 45.559 47.559 47.559	24.24.24.24.24.24.24.24.24.24.24.24.24.2	61.559 65.559 67.559 67.559	71,554 73,548 77,5473 77,567	80.952 84.223 84.223 85.616	86.0055 89.0018 89.0018 90.640	92.04.092.95.095.095.095.095.095.095.095.095.095.	95.996 96.528 97.591 97.591	99.596 99.219 99.888 188.148 180.452	180.719 180.949 181.142 181.482	161.539 161.613 101.674 101.724	181.840 101.840 181.865 101.890	101.931
56.378 52.378 54.873 56.873	864.44 844.44 844.44 844.44 864.44	78.474 72.474 74.674 76.474 76.474	5000 0000 0000 0000 0000 0000 0000 000	98.364 92.346 94.246 96.159 97.936	99.604 101.149 102.548 103.769	106.234 107.958 109.916 119.596	111,234 112,151 113,678 113,996 114,685	115.743 116.677 117.549 118.158	119-671 119-678 119-678 128-893	128.185 128.279 120.354 128.419	120.515 128.557 120.631 120.664	126.702
962.23 962.23 962.23 962.23	24.296 56.296 58.296 58.296 68.296	64.246 66.256 69.296 70.296	74.292 76.275 78.228 80.135	93.762 95.465 67.435 68.688 89.913	91,107 92,195 93,195 53,965 94,771	95.966 97.564 99.356 98.946	99.946 100.547 101.155 102.292	103.615 103.615 104.683 104.683	105.684 105.684 105.849 106.866	196.418 106.544 106.645 106.724	105.836 105.438 105.915 105.948	166.994
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55.580 60.580 62.580 64.580	66.56	76.580 78.580 80.580 82.580	86. 580 90. 588 92. 588 94. 588	96.500 96.498 100.450 182.415	146.067 107.779 109.351 110.765	115.589 116.835 117.746	119-763 128-636 121-925 122-987 124-025	125.068 126.289 127.404 129.126 129.772	129.367 129.599 130.378 130.789	131.657 131.657 132.677 132.031	132,256 132,349 132,426 132,494 132,594	132.611 t by (\$/cm²),
65.876 67.076 69.076 71.476 73.876	75.076 77.076 79.076 51.076	85.076 87.076 39.076 91.076	95.076 97.075 99.076 141.076	105.976 137.076 109.076 111.076	115.076 117.066 119.007 120.001	124.547 126.501 128.561 129.578 131.059	132.615 136.216 135.848 137.458 139.848	148.603 142.222 143.731 145.001	147.040 147.335 149.685 149.195	150.056 150.324 150.532 150.693 150.613	150.906 150.908 151.049 151.105	151.196 breviated her
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77.654 73.654 81.656 53.656	64 93.65 91.65 91.65 91.65 91.65	97.654 93.654 101.654 103.654 105.654	107.654 103.654 111.654 113.654 115.654	117.654 119.654 171.654 173.654 173.654	127.654 133.654 131.654 133.654 133.654	137.654 139.654 141.656 145.656	167.591 169.577 151.577 153.575 153.575	157.552 153.539 161.486 163.329 163.030	165.731 168.264 169.659 170.905	172.962 173.715 174.317 174.812 175.255	175.556 175.075 176.072 176.253 176.425	176.577 of u ate mol
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	E-30 E-45. 16-45. 0-00125 0-50000 0-500188			6.6 6.6 6.5 6.5 6.5 6.5 6.5 6.5 6.5 6.5	6.686 0.972 1.067 1.187	1.5545 2.0554 2.0554 2.0554 2.0554 2.0554 3.05554 3.05554 3.05554 3.05554 3.05554 3.05554 3.05554 3.05554 3	50000000000000000000000000000000000000	7 - 2 3 0 5 - 3 7 3 9 - 4 8 1 10 - 6 3 5 11 - 6 2 2
	1.000000 1.000000 1.000375 3.095E 19			######################################	4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	1.470 2.071 2.025 2.443 2.443 2.443	8.577 6.336 9.228 7.334	00000000000000000000000000000000000000
dν	L109 243+ 3291+ 0+5300 0+003750 0+003922- 5+706E-19	변 ed (5) 2 에 여 전 한 전 한 약 한 전 이 가 가 한 전 이 다 한 전 이	8 . 126 8 . 149 8 . 172 8 . 191 8 . 256		1199-00 0000 0000 0000 0000 0000 0000 00	6.617 6.975 1.675 1.113	######################################	2.218 2.495 2.714 2.984 3.155
y A y	L107 245. 3291. 0.03850 0.015395 5.847E 19	는 OP () 여 PP () 다 이 이 이 다 이 이 이 다 이 이 이 다 이 이 이	0 + 1 + 1 + 1 + 1 + 1 + 1 + 1 + 1 + 1 +		0.00 10.00 11.00 10.00 1	44444444444444444444444444444444444444	22.22.22 22.22.23 23.23.23 23.23.23 23.23	3.729 4.218 5.618 5.618 5.428
LE 25	L105 245- 1646- 0-01910- 0-062105 0-062461 5-860E 19	(C) (A) (A) (A) (A) (A) (A) (A) (A) (A) (A	0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000	6.547 0.641 0.714 1.195	1.554 1.664 1.664 1.666	2,165 2,472 2,615 4,093 2,155	WA THE	6.50 4.50 4.50 5.00 5.00 5.00 5.00 5.00 5
TABLE	E-103 2-46. 16-46. 0-00500 0-250000 0-250375 6-100E 19		6 . 3 4 4 4 6 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	0 - 7 3 8 8 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9	2.0055 2.0055 2.0055 2.0055 5.0055 5.0055	25.74 25.74 25.74 75.74 75.74 86.94	5.045 5.045 7.669 4.22	0.000 0.000
	L101 245- 1648- 0.00125 1.000000 1.000375 6-175E 19	9 P P S P P S P P S P P S P P S P P P S P	900000000000000000000000000000000000000	4.00 4.00 4.00 4.00 4.00 4.00 4.00	8	4 . 591 4 . 583 5 . 266	2442 2442 2442 2442 2442 2442 2442 244	13.805 15.515 17.516 18.961 28.727
	LH06 244- 3291- 0-15390 0-007500 0-007844	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	2 - 1 - 1 - 2 - 2 - 2 - 2 - 2 - 2 - 2 -	NO MON S	1.0856 1.153 1.222 1.299	1.587 1.587 1.639 1.792	2-171 2-392 2-925 3-256	7.00 7.00 7.00 7.00 7.00 7.00 7.00
	LH06 245. \ 3291. 0.030921 0.031278	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6		1.693 1.693 1.6775 2.805 2.168	2.22.22.24.24.24.24.24.24.24.24.24.24.24	4.00 4.00 5.00 5.00 5.00 5.00 5.00 5.00	6.946 7.831 8.591 9.591
	LH04 245- 1648- 0-01910 0-12348- 0-12493	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 . 3 4 4 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	2.528 2.528 2.683 2.859	5 4 4 5 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	6.164 7.112 7.712 9.664	10.947 12.255 13.471 14.731 16.826
	LMGE R43: 1648: 0.00500 0.50000 0.500750 1.245E 20	# # # # # # # # # # # # # # # # # # #	- 100 mm m	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	96464 64664 4464 7664 7664 7664	0.000 m	90000000000000000000000000000000000000	15.776 13.568 28.317 22.110 23.927
	Sam. No. Temp (K) Path (cm) Conc. P (atm) P (atm) U (\$/cm^*)*	(cm ⁻¹) 596.80 592.88 594.80 594.80	6002. 6002. 6004. 6006. 6006.	616.86 612.86 614.80 616.80 616.80	622.00 622.00 624.00 626.00 626.00	642.00 642.00 644.00 646.00 646.00	640.00 642.00 644.00 646.00 646.00	655 655 655 655 655 655 655 655 655 655

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	1.602	1.712	2.827	424.2	3.210	3,437	3.562	3.681	3.802	7,925	7.00	4.4.5	4.256	4.346		4.44	4.525	4.536	4.635	4.709	4.757	4.80		N 1 8 4 9	206*		4.925	4.945	900	N C C C C C C C C C C C C C C C C C C C	20.40	5.857	5.157	5.202	5.217		5.242	5.254	7074	2.65							
	2.971	3.179	3.730	4.254	5.378	5.814	6.051	6.286	6.528	6.751	4. 977	**************************************	7.447	7.579		7.757	7.931	9.076	8.283	6.314	6.44	10	566	A.6.48	3.667		8.734	8.788	5 1 1 C	2004		8.969	9.159	9.230	9.249		9.291	9.313	9.50	***							
	5.242	\$.63¢	6 - 1 V 4	7.216	8.651	9.369	3.834	11.279	18.731	• • • • •	11011	11 .014	707.4.	12.7.2		13.856	13,356	13.616	13 • 8 42	34.845	16.215	192.41	10000	605.4	14.688		14.766	14.635	10.00	896°41	14.365	15.121	15.448	15.532	12.557		15 .618	15.654	15.638	15.785							
	955.8	9.291	18.668	11.613	13,332	14.446	15.218	15.992	16.796	17.593	18.378	40.10	19.784	20.488		58.969	21.495	21.959	22.386	22.754	878 26	24. 280	24.564	23.719	23.877		24.818	24-119	24.213	692-42	2000	24.522	24.993	25.145	25.178	;	25.278	25.341	52.404	454.62	-						
	13.801	14.135	15.255	17.625	19.513	20.965	22.25	23.497	24.793	26.046	27.358	28.565	29.7.11	30.772		31.759	12.661	32.465	34.176	34.791	16. 110	32.34	37.192	36.395	36.625		36.884	36.944	37.052	37.136	31.02	37.486	37.942	36.185	36.139		36.237	38.256	36.365	155.8							
	15.675	17.281	13.916	21.584	23.643	25 . 114	29.92	28.168	29.739	311.307	MS 9 - A.S.	34.357	167.35	37 - 157		38.425	33.595	41.645	41.572	42.372	370 27	13.647	10.000	44.376	44.638		46.835	44.984	100 100	582.64	45.645	45.688	46.827	145.24	46.288 46.734		281.34	16.476	45, 554	46.592							
	3.372	3.951	4.227	4.603	5.944	6.391	6.65	70.0	961.)	7.411	7.657	7.696	9.106	9.305		9.506	6000	570	6.76	16.6	9.193	9.277	9.356	9.420	9.484		9.536	2/6	244	9.684		9.765	\$ 958	18.045	10.182		18.136	10.101	18.226	10.254	18.243	10.327	10.34	16.597	18.428	18.440	•
	5.832	6.813	7.264	7.998	9.446	10.173	129.01	11.4	11.532	11.988	12-429	12.849	13.236	13.581		13.916	14.23	D	14.7.6	14.363	15.185	15.258	15.480	15,523	15,622	1	15.708	19001	15.899	15.953		16.093	16.426	16.539	16.596		129.61	16.786	16.739	16.774	66.489		16:984	16.934	16.956	16.975	
	10.325	11.964	12.690	13.720	15.455	16.573	17.586	10.01	19.450	19:69	28.780	21.463	22.163	25.792		23, 393	166.52	7		177.67	25.608	25.884	26.132	26.344	26.522		26.677	210.02	27.828	27,123	,	27.374	27.921	22.02	28.188		26.258	28.305	26.466	28.535	28.598	24.674	29.746	28.792	20.631	26.863	
	15.928	16.436	19.586	20.960	22.868	24.496	25.631	0/11/2	666.83	29.895	31,224	32.500	33.708	34.834	;	35.590	20.02	20.00	****	23.66	39.679	40.406	46.658	41.241	41.562		40.00	000000	42.39	42.513		42.792	43.525	43.772	43.586		900.44	44.746	64.329	44.432	44.534	44.5	***751	44.819	44.871	44.915	
	28.493		27.587	•	31.395	m ı	^ .			•	N	•	45.961	ĸ		49.255	20.10	22.162	200	24.034				57.674		-4	58.509		• •	٠.			-		61.014		61.143			61.724			62.118			62.325	
•	6.131	7.161	7.677	9.482	9.469	10.656	11.136	610 67	76.037	12.573	15.038	13.481	13.885	14.248	:	14.609	****	120 552	1000	12.000	15.868	16.021	16,159	16.288	16.374	•	16.454	10.263	16.628	16.674		16.889	17.144	17.253	17.295		17.319	7.757	17.39	17.414	17.44.5	17. 608	17.550	17.573	17.598	17.667	by (4/c=2)
	16,956	12.701	13,560	14.598	16.336	17.545	18.40	19.60	961.82	26.989	21.825	22.619	23,848	24,003		24.643	962.62	20,000	*63.00	900.00	27.023	27.336	27.616	27.651	28.040	;	28.215	200.00	26.596	28.781		28.956	29.543	29.744	29.863		29.936	111000	30.166	30.241	X8. X28		30,532	30.589	36.638	34.683	reviated here
	17,317	19.913	21.208	22.631	24.540	26-168	27.516	2000	54.2 · B2	31.595	32.918	34.185	35,379	36.49	1	37.546	450.00	23.453		006-	41.588	42.127	42.603	43.065	45,337		43.523		16.26	44.425		44.822	45.635	878.CP	46.061	:	46.179	46.4.34	46.560	46.681	46.798	46.044	47.078	47.159	47.238	47.291	ules/cm2, abb
	25.748	24.54	31.113	32.937	34.979	36.916	38 - 768	70.	/ ** 7 *	848.49	46.19A	48.823	49.845	51.530		53.169	24.762	#12.0C	100000	28.708	59.878	68.85	61.653	62.357	856.39		63.458	2000	61.5.49	69.79		65.259	66.223	66.563	75 E - 49		67.038	277 47	67.679	67.686	68.83	100.19	68.486	69.612	68.711	68.798	of u are molecules/cm, abbreviated here
	650.00	664.00	666.00	668.00	670.00	672.00	674.80		04.879	680.80	682.00	684.80	686.00	688.00		690.00	01.269	D • 9 50 0	0.000	980.08	700.80	702.80	704.80	706.00	703.00		710.60	717.00	716.80	718.00	,	720.00	722.11	724.10	726.00		730.88	734.00	736.00	738.88	710.00	26.24	744.80	746.00	748.00	750.00	* The units

	LN02 646. 6125 0125 11316 11328						*60		1.527 1.724 1.922 2.029	2.131						
	LMOE 845- 1646- 0-031316 0-031328 1-934E 18	-					••	-000-		N						
	1.924 0.00.02 0.00.02 0.0022 0.0022 0.0022 0.0022 0.0022	-					 -119	0.484 0.464 0.467 0.959	7.00 to 0.00 t	2.589						
	1646. 0.00500 0.015681 0.015681 3.6561				*			0.157 0.237 0.437 0.437	2.00 t to t	2.278						
	1.802 2.85. 1.645. 0.00125 0.062500 0.068500 0.068500						, , , ,	0.32¢ 0.47¢ 0.640 1.25¢	2.278 2.591 2.761 2.941							
	0.00125000 0.125000 0.125000						0.	# 00 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	2.762 3.176 3.617 3.669 3.981	**193	,					
	16.06 0.01910 0.00743 0.00743		776 e 6 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	40000	0 .213 0 .237 0 .267		0.769 0.986 1.0852 1.196	62-1 1-39-2 2-62-1 2-62-2 1-62-2 2-62	90000 90000 90000 90000 90000 90000 90000	20004 2000 2000 2000 2000 2000 2000 200	\$1484 50074 60074 60074	6444 6444 6444 6444	00000 00000 00000 00000 00000 00000	1,000	1111 0000 0000 0000	
ηp	LL04 245- 1646- 0-00500 0-031316 0-031363 7-735 18 7		000000000000000000000000000000000000000	0.237 0.242 0.254 0.254 0.295	0.129	0.644 0.950 0.970 1.120	2.6.2 2.6.2	966.5 996.5 996.5 996.5 996.5	6.959 5.1569 5.116 5.376	5.199 6.218 6.218 6.319 6.319	6.984 6.994 7.188	7.00 4.00 4.00 4.00 7.00 7.00 7.00	7.508 7.531 7.551 7.566	7.000	7.859 7.966 7.976 7.978	
BLE 26 /A	0.00125 0.00125 0.125047		0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	0.263 0.273 0.289	8 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	1.957 2.308 2.630 2.961 3.502	4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	6.55 7.55 7.55 7.55 7.55 8.25 8.25 8.25 8.25 8.25 8.25 8.25 8	9.661 9.020 9.030 9.715 10.01	10.279 10.521 10.733 11.066	11.199	11.566 11.596 11.623 11.663	11.964	11.993 12.005 12.021 12.030	
	LL01 244. 824. 0.00125 0.250000 7.704E 18		0.000 000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.		0000 AV	E	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	6 11 12 12 12 12 12 12 12 12 12 12 12 12	2000 2000 2000 2000 2000 2000 2000 200	24 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	13.00% 13.4626 13.415 14.965	**************************************	116.794	15.203 15.203 15.203 15.203	15.228	
	243. 243. 3291. 0.03850 0.003860 0.003860		0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 1196 0 219 0 229 0 225 0 275 0 276	3 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	8 9 8 8 8 9 9 9 8 9 9 4 9 9 8 9 4 9 9 8 9 4 9 9 9 9 4 9 9 9	2684 2684 2684 2684 2684 2684 2684 2684		5555 5400 5400 5500 5500 5500 5500 5500	3444 6624 3050 3050 3050	M F F F F F F F F F F F F F F F F F F F	5.00 5.00 5.00 5.00 5.00 5.00 5.00 5.00	5.176 5.176 5.119 6.119	25.50 25.50 25.50 25.50 25.50 25.50	7
	LK06 245- 1646- 0-01910 0-01586 0-015615		0.0821	**************************************	00.54 44.7 10.54 1	00 00 00 00 00 00 00 00 00 00 00 00 00	1.654 2.191 2.299	2.69. 2.69. 3.09. 3.00.	4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	6.646 6.646 6.646 7.6646 7.6646	7-1197 7-186 7-582 7-599	7.000 7.000 7.000 7.000 7.000 7.000		6.20 6.20 6.50 6.50 6.50 6.50 6.50 6.50 6.50 6.5	9.576 9.593 9.613	by (4/cm²).
	LK04 245. 1646. 0.00500 0.06250 0.062594		00000 00000 00000 00000	00000 144 144 144 144 144 144 144 144 14	000000 00000 00000 00000 00000	2000 2000 2000 2000 2000 2000 2000 200	1825 1825	6.14 5.14 5.014 6.016 6.016	9.054 9.127 9.143 9.572	11000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000	1122 1122 1122 1123 1123 1123 1123 1123	13.410 13.555 13.555 13.655	11 12 13 13 13 13 13 13 13 13 13 13 13 13 13	16.234 16.534 16.639 16.665	16.725	reviated here
	LKOE 845. 1646. 0.00125 0.250000 0.250094		000000000000000000000000000000000000000	000000000000000000000000000000000000000	00.00 00	25.20 25.20	6 5 2 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	7.105 7.726 6.364 9.780	12.457	15.344 16.757 17.391 17.962	10.495 19.4964 19.784 20.065	20.326	21.054 21.116 21.1167 21.282 21.233	21.33 21.7660 21.753 21.765	21.505 21.531 21.562 21.674	molecules/cm ² , abbre
	EX5. 845. 0.00125 0.500100 0.500100 0.500100		6.0 2.0 2.0 4.101 2.001	2004 2004 2004 2004 2004 2004	8.882 8.928 1.679 1.590	4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	5.649 5.649 5.451 5.451	3.047 9.672 13.656 11.362	16.211 16.316 16.316 17.263	19.213 21.675 21.938 22.713	\$2.45 \$2.45 \$2.45 \$4.45	25.92 25.631 25.631 25.631 25.631 25.631	26.946 26.992 27.064 27.064	27.216 27.549 27.696 27.696	27.745 27.701 27.915 27.93	of u are solec
	Sam. No. Temp '4.) Path (cm) Conc. P (atm) U (((cm))*	(ca1)	612.00 612.00 614.00 615.00 615.00	00000000000000000000000000000000000000	20000000000000000000000000000000000000		6556.00 6556.00 6556.00 6556.00	666.00 666.00 666.00 666.00 666.00	674.40 672.80 574.88 675.00 675.00	2000 2000 2000 2000 2000 2000 2000 200	692.00 694.00 696.00 695.00	700.000	710.80 712.00 714.00 716.80	720.86 725.86 726.86 726.86	730.00 732.00 735.00	* The units

Sam. No. Temp (K) Path (cm) Conc. P (atm) P (atm) u (#/cm²)*	LP01 249• 3291• 1•00000 0•769737 1•000658 7•471E 22	TABLE	27	Sam. No. Temp (K) Path (cm) Conc. P (atm) P (atm) u ^e (#/cm ²)*	LQ01 249• 3291• 1•00000 0•769737 1•000658 7•471E 22
(cm ⁻¹)				(cm ⁻¹)	
500.00	1.	-11		7 5 0 • 0 · G	0.
502.00	0.015 0.049	{ [782.00	0.552 1.056
504.00 506.00	0.045			734•00 736•00	1.493
508.00	0.114	-11		788.00	1.884
		11	•		
510.00	0168	-11		790.00	2.230
512.00	0.197 0.230	[]		792 .0 0 794.00	2 • 8 5 9 3 • 9 7 1
514.00 516.00	0:.269			796•00 796•00	4.669
518.00	9:.328	-		798.00	5.091
J13000				, , , , , ,	
520.00	0.402	11		300.00	5.532
522.00	0 • 4 85			902.00	5.997
524.00	0:.584	-11		304.00	6.470
526 .0 0	0706	11.		806•00 808•00	6.940 7.382
528.00	0.862			20200	1 40 32
530.00	1.012	11		810.00	7.796
532.00	1.171			812.00	5.177
534.00	1.334	11		314.00	3,507
536.08	1.500	11		816.00	6. 799
538.00	1 • 6 6 5			815.00	9.051
540.00	1.798			820.00	3.257
542.00	1.914	11		822.00	9.431
544.D0	2.089	:		824.00	9.530
546.00	3.256	11		826 .0 0	9.708
548.00	3.756	-]]		828.00	^ , d-33
550.00	3.960	11		530.00	9.966
552•00	4.183	l l		332.00	10.066
554.00	4.426			834.00	10.140
556.00	4.709	ii ii		936.00	10.222
559.00	5.019	11		838.00	10.292
	- 754	ll l			40 770
560.00	5.356			840.00	10.368
		, 2		942.00 844.00	10.446 10.521
* The units	of u are molecule	es/cm ,		846.0.Ü.	10.521
abbrevist	ed here by (#/cm²	١, ۱		848.00	10.644
	or nove sy (") oill	′′			
		11		850.00	10.703



transmittance of several ${\rm CO}_2$ samples near 310 K. Spectral plots of Figure 10.

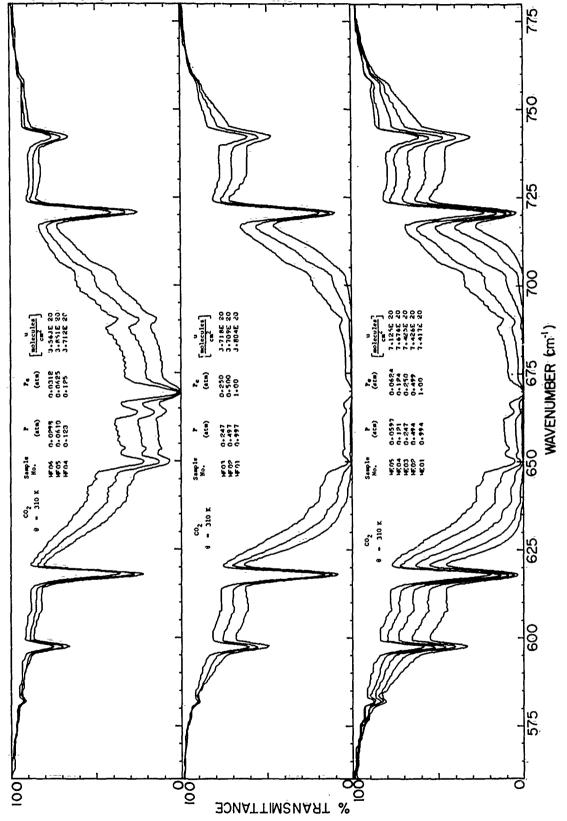
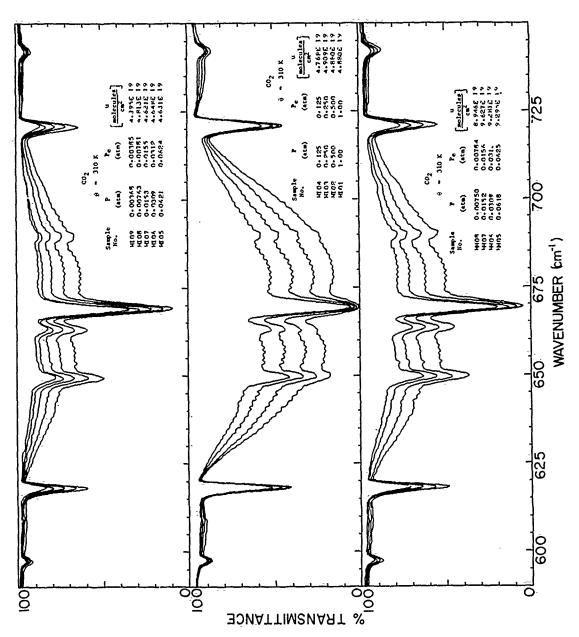


Figure 11. Spectral plots of transmittance of several ${\rm CO}_2$ samples near 310 K.



Spectral plots of transmittance of several ${\rm CO}_2$ samples near 310 K. Figure 12.

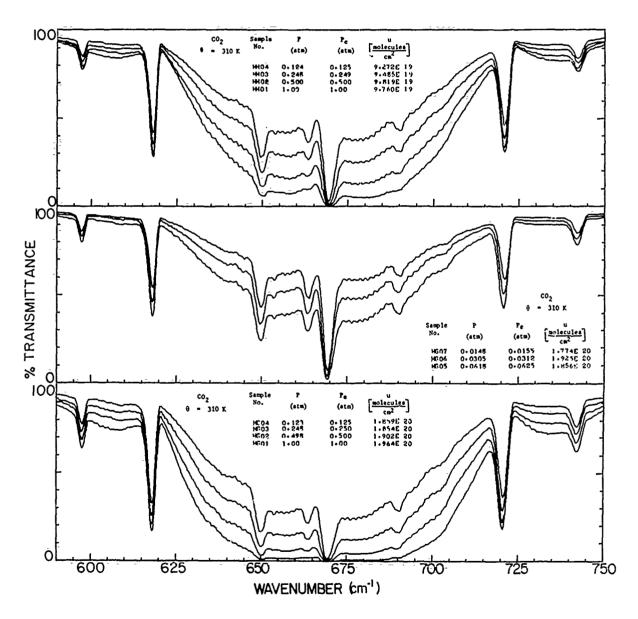


Figure 13. Spectral plots of transmittance of several ${\rm CO}_{\bar{2}}$ samples near 310 K.

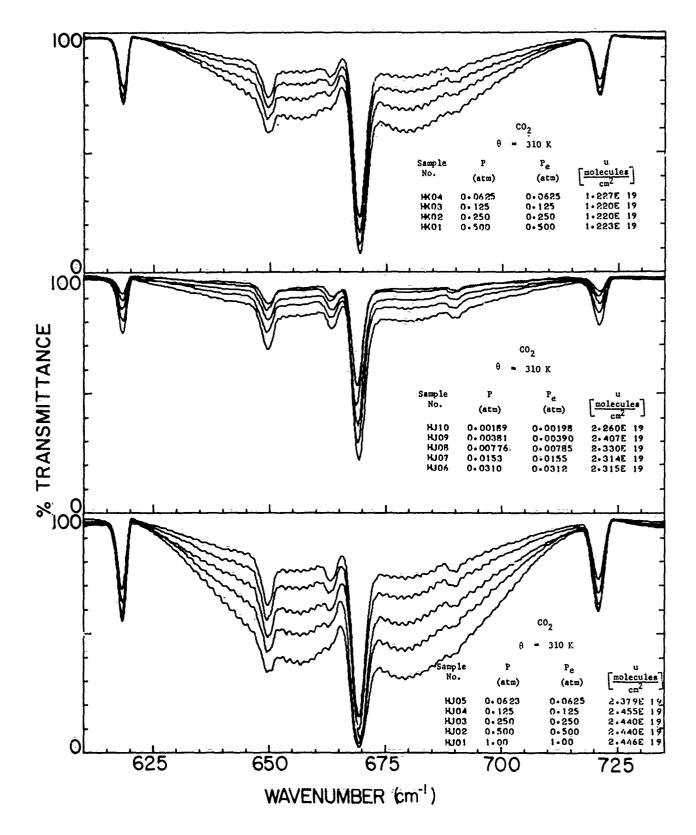


Figure 14. Spectral plots of transmittance of several CO₂ samples near 310 K.

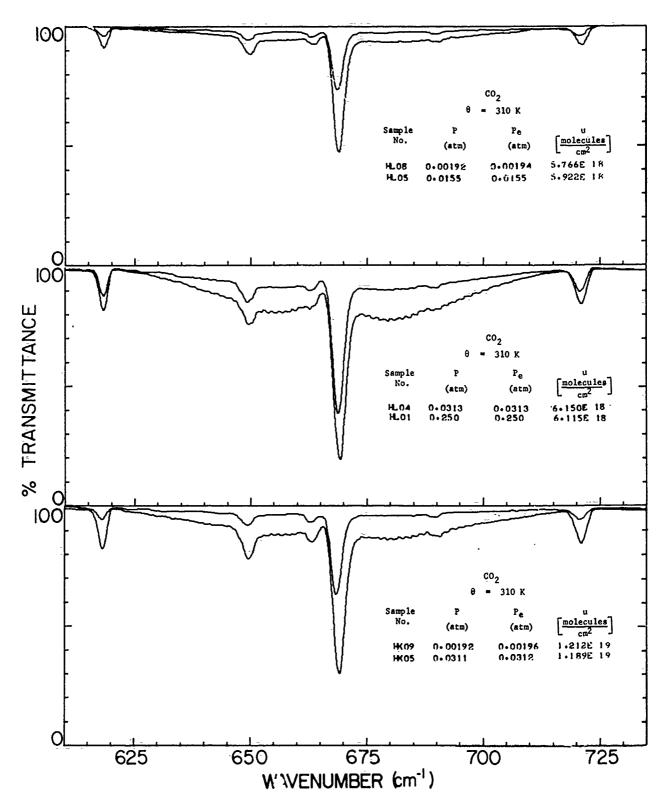
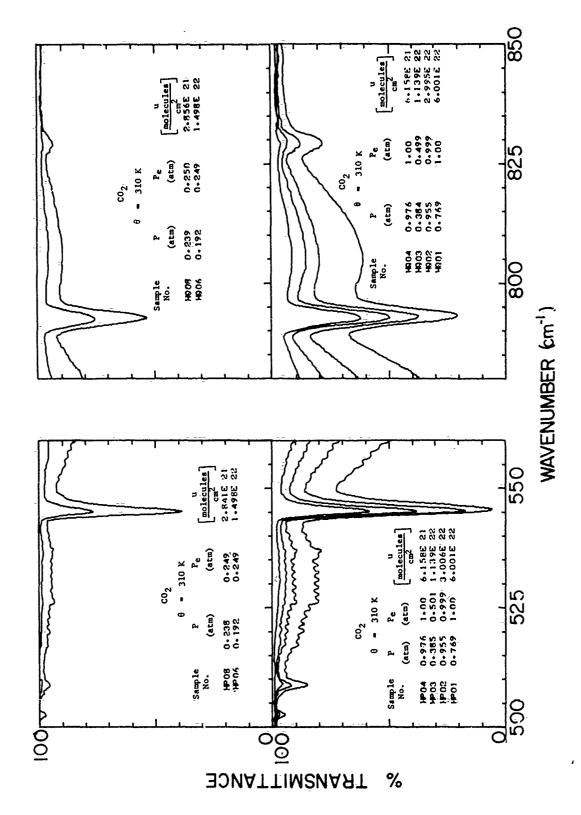
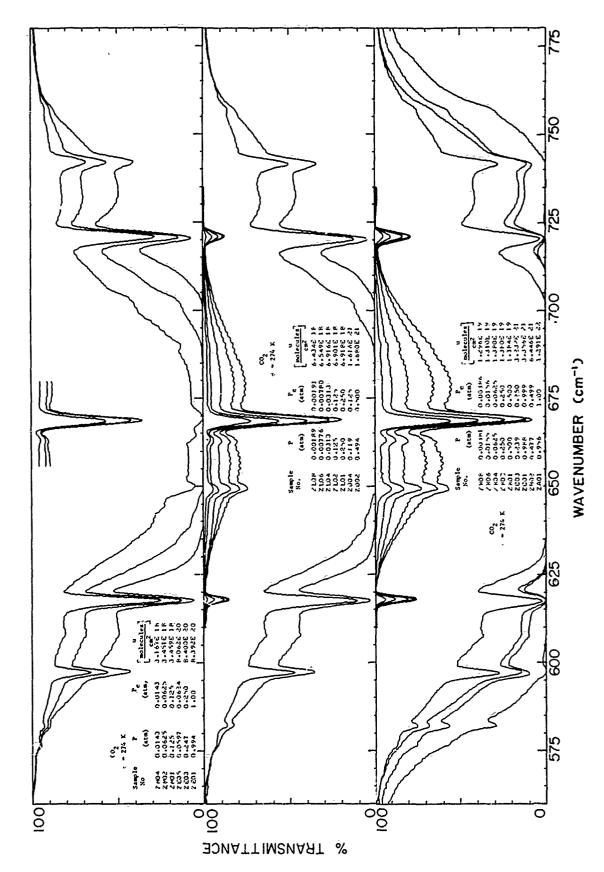


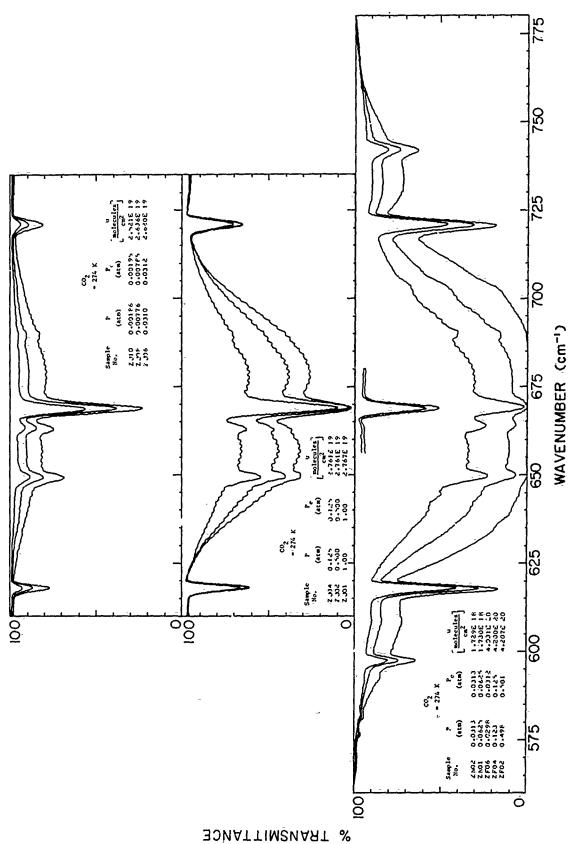
Figure 15. Spectral plots of transmittance of several ${\rm CO}_2$ samples near 310 K.



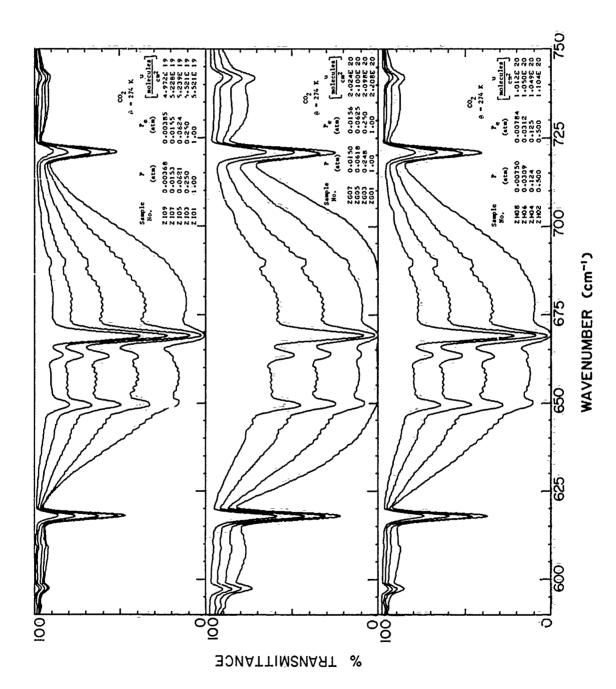
Spectral plots of transmittance of several ${
m CO}_2$ samples near 310 K, Figure 16.



Spectral plots of transmittance of several CO_2 samples near 274 K. Figure 17.



Spectral plots of transmittance of several ${\rm CO}_2$ samples near 274 K. Figure 18.



Spectral plots of transmittance of several CO_2 samples near 274 K. Figure 19.

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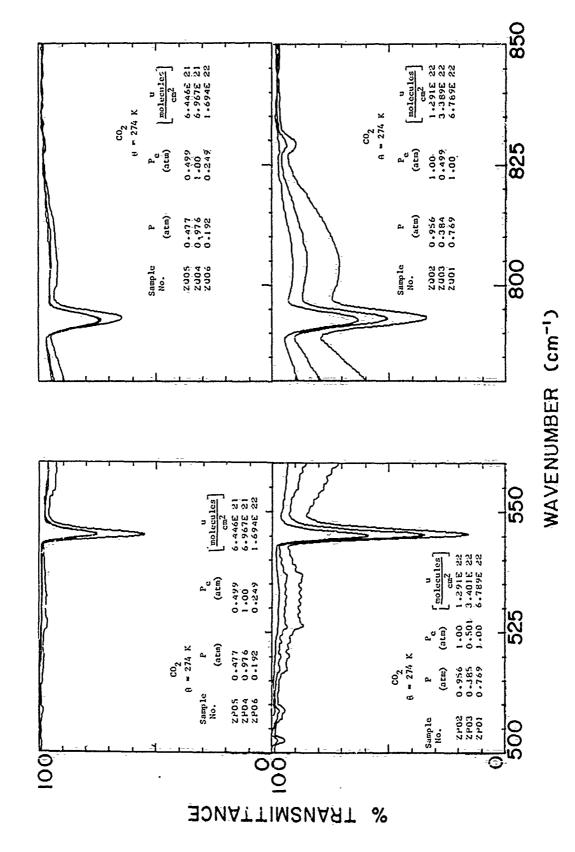


Figure 20 . Spectral plots of transmittance of several 60 samples near 274 K.

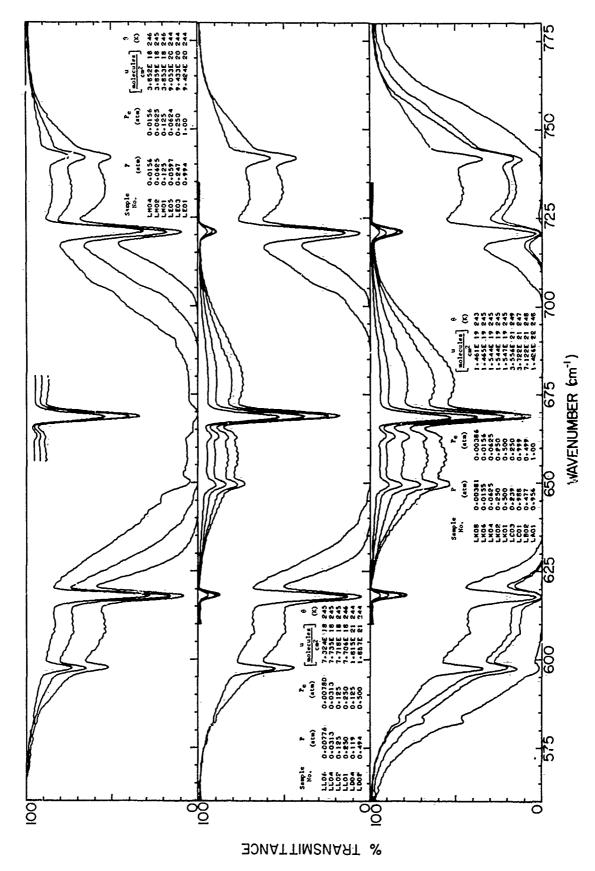
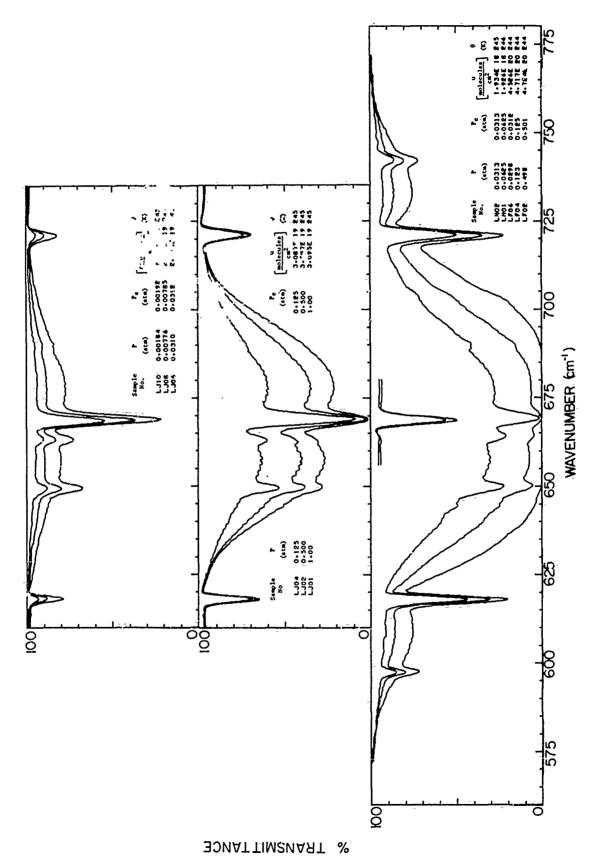
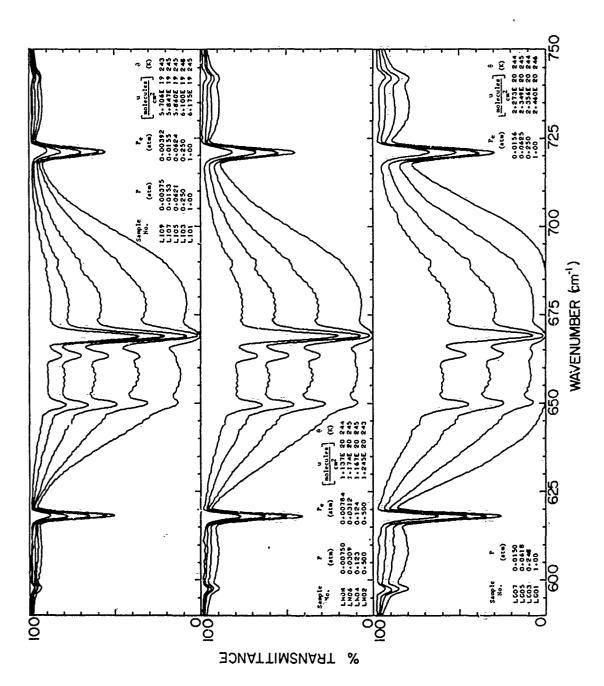


Figure 24. Spectral plots of transmit for a several CO₂ samples near 245 K.



Spectra. plots of transmittance of several ${\rm CO}_2$ samples near 245'K, Figure 22.



Spectral plots of transmittance of several CO_2 samples near 245 K. Figure 23.

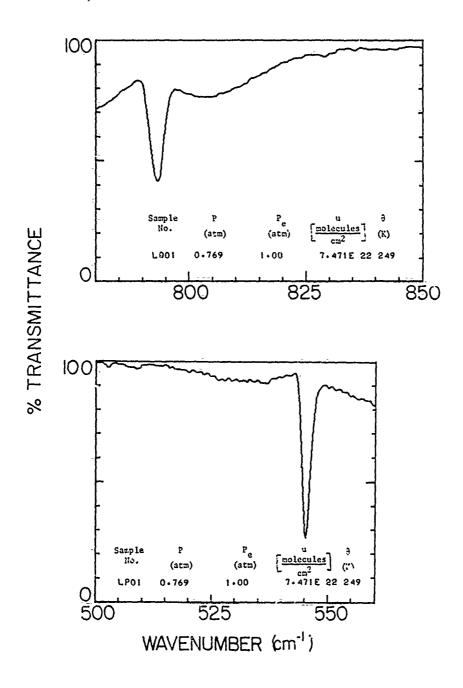


Figure 24. Spectral plots of transmittance of several ${\rm CO}_2$ samples near 245 K.

SECTION 6

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